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MATERIAL PROPERTIES DESIGN USING SIMULATIONS AND EXPERIMENTS  
FOR POWDER INJECTION MOLDING OF LEAD ZIRCONATE TITANATE (PZT)

By  
Bhushan Pramod Bandiwadekar  
B.E Mechanical, University of Mumbai, 2015  
PGDTD&CC, MSME, Indo German Tool Room, 2016

A Thesis  
Submitted to the faculty of the  
J. B. Speed School of Engineering of University of Louisville  
In Partial Fulfillment of the Requirements  
for the Degree of

Master of Science  
in Mechanical Engineering

Department of Mechanical Engineering  
University of Louisville  
Louisville, Kentucky

December 2017

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A Thesis Approved on

November 30, 2017

by the following Thesis Committee:

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Dr. Kunal Kate

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Dr. Sundar Atre

---

Dr. Jagannadh Satyavolu

## DEDICATION

This thesis is dedicated to my parents

Mr. Pramod Arjun Bandiwadekar

and

Mrs. Pradnya Pramod Bandiwadekar

who have given me invaluable educational opportunities

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Researchers are sometimes told, “Get a life!”, and I have one, thanks to my friends Juili, Muddasir, Sonali and many more from my circle of friends for their goodwill, support and guidance through numerous tough decisions. With ambitions soaring high, I relied on them to strike a balance between work and leisure.

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Bhushan Bandiwadekar



## ABSTRACT

### MATERIAL PROPERTIES DESIGN USING SIMULATIONS AND EXPERIMENTS FOR POWDER INJECTION MOLDING OF LEAD ZIRCONATE TITANATE (PZT)

Bhushan Pramod Bandiwadekar

November 30, 2017

Powder injection molding (PIM) process simulations can be performed to minimize the number of injection molding experiments by estimating material properties necessary for PIM simulations. In current work, lead zirconate titanate (PZT) powder-polymer binder feedstock was compounded for 45 vol. % and 52 vol. % solids loading. PIM experiments on designed micro-pillar array geometry were performed using 52 vol. % PZT. Using PIM experiments results as basis, PIM simulations were performed on designed micro-pillar array geometries to understand the effectiveness of PIM simulations with the use of estimated feedstock properties in predicting molding behavior that have micro-features. Additionally, PIM simulations were performed to understand the defects after debinding and sintering. As the approach is to develop feedstock without measurement of feedstock properties, it is expected that the results from current work will help in reducing the number of experiments needed to obtain a defect free PIM products.

## TABLE OF CONTENTS

Acknowledgements.....	iv
Abstract.....	vi
List Of Tables .....	ix
List Of Figures .....	xi
1. Introduction.....	1
2. Influence Of Feedstock Property Estimates And Measurements On Powder Injection Molding Of Lead Zirconate Titanate (Pzt) .....	5
2.1. Introduction.....	5
2.2. Experimental Materials And Methods .....	7
2.3. Results And Discussion .....	9
2.3.1. Estimating Properties Of Powder-Polymer Mixtures.....	9
2.3.2. Experimental And Simulations Results.....	15
2.4. Summary.....	19
3. Influence Of Feedstock Property Estimates And Simulations On Powder Injection Molding Of Lead Zirconate Titanate (Pzt) Microarrays.....	21
3.1. Introduction.....	21
3.2. Experimental Materials And Methods .....	22
3.3. Results And Discussion .....	24
3.3.1. Estimating Material Property .....	24

3.3.2.	Experiments And Simulations .....	28
3.4.	Summary .....	37
	Conclusions .....	38
	Future Work .....	39
	References .....	40
	Appendix .....	44
	(A) Cad Models And Process Conditions For Simulations .....	44
	(B) Effect Of Change In Microarray Spacing .....	47
1.	Mold Filling Behavior .....	47
2.	Air Traps .....	48
3.	Powder Concentration .....	48
	(C) Effect Of Change In Gate Location .....	49
1.	Mold Filling Behavior .....	49
2.	Air Traps .....	49
3.	Powder Concentration .....	50
4.	Shear Stress .....	51
	(D) Rheology Of Powder-Polymer Composite .....	53
	Curriculum Vita .....	57

## LIST OF TABLES

TABLE	PAGE
Table 1: PZT powder properties .....	7
Table 2: Solid and melt densities of feedstocks with 45 vol. % PZT powder .....	10
Table 3: Specific heat capacity and thermal conductivity values at various temperatures for feedstocks with 45 vol. % PZT powder .....	11
Table 4: Dual-domain Tait constants for feedstocks with 45 vol. % PZT powder.....	12
Table 5: Cross-WLF constants for feedstocks with 45 vol. % PZT powder .....	14
Table 6: Data set used for simulations.....	16
Table 7: Statistical comparison of experiments compared with simulations using estimated and hybrid material properties (a) relative error in part weight of simulations w.r.t. experiments (b) Volumetric shrinkage (%) of base plate .....	19
Table 8: Process conditions for powder injection molding .....	24
Table 9: Solid and melt densities of feedstock with 52 vol. % PZT powder.....	25
Table 10: Specific heat capacity and thermal conductivity values at various temperatures for feedstock with 52 vol. % PZT powder .....	26
Table 11: Dual-domain Tait constants for binder and 52vol% PZT feedstock .....	27
Table 12: Viscosity constants .....	28
Table 13: Comparison of part weight with experiments and simulations .....	30
Table 14: Comparison of linear shrinkage in experiments and simulations.....	30

Table 15: PIM process conditions.....	46
Table 16: Measured viscosity of 52 vol. % PZT with WB50 multicomponent binder ....	53
Table 17: Measured viscosity of WB50 multicomponent binder .....	54

## LIST OF FIGURES

Figure 1: SEM image of PZT powder.....	7
Figure 2: Rectangular plate (a) Solidworks part file (b) Meshed with runner gate system in Moldex3D Designer.....	9
Figure 3: PVT behavior for 0, 100, and 200 MPa pressures for 45 vol. % PZT powder.	12
Figure 4: Comparison of viscosity with shear rate at different temperatures for 45 vol. % PZT powder. ....	14
Figure 5: PIM experiment for 45 vol. % PZT rectangular plate with 100% filling at injection velocity 90 mm/s and injection pressure at 40 MPa (a) top view (b) 3D perspective view.....	16
Figure 6: Moldex3D simulation for 0.45% PZT base plate - 100% filled at injection velocity 90 mm/s: (a) 30% filled in 0.025s, (b) 45% filled in 0.038s, (c) 75% filled in 0.064s and (d) 100% filled in 0.085s .....	17
Figure 7: Evolution of simulated flow front for 0.45% PZT base plate compared with experimental results .....	18
Figure 8: Experiments compared with simulations using estimated and hybrid material properties - (a) Part weight of base plate (b) Volumetric shrinkage (%) of base plate.....	18
Figure 9: Microarray geometry: SolidWorks part file .....	23
Figure 10: Meshed in Moldex3D designer .....	23

Figure 11: Sintered Microarray part .....	29
Figure 12: Mold filling behavior in microarray .....	30
Figure 13: Powder concentration of filled and packed microarray.....	31
Figure 14: Powder concentration within individual micro-pillars.....	32
Figure 15: (a) Powder concentration of micro-pillar at location A1 (b) Broken micro-pillar .....	33
Figure 16: Temperature during filling at bottom of micro-pillar.....	34
Figure 17: 3D plot of temperature distribution within micro-pillar with respect to its distance from gate location.....	34
Figure 18: 3D plot of % powder concentration with respect to its distance from gate location.....	35
Figure 19: Flow chart for simulations.....	44
Figure 20: Microarray geometry (CAD model) with inter-pillar spacing (a) 0.7 mm (b) 1.2 mm (c) 1.7 mm.....	45
Figure 21: Bottom gate location on the mesh file (Moldex3D).....	46
Figure 22: Mold filling behavior for change in microarray spacing.....	47
Figure 23: Air traps for change in microarray spacing.....	48
Figure 24: Powder concentration for change in microarray spacing .....	48
Figure 25: Mold filling behavior for change in gate location.....	49
Figure 26: Air traps for change in gate location .....	49
Figure 27: Comparison of air traps for different gate location .....	50
Figure 28: Powder concentration for change in gate location .....	50
Figure 29: Shear stress for 0.7 mm microarray spacing with bottom gate .....	51

Figure 30: Shear stress for 1.2 mm microarray spacing with bottom gate .....	51
Figure 31: Shear stress for 1.7 mm microarray spacing with bottom gate .....	52
Figure 32: Measured viscosity of 52 vol. % PZT with WB50 multicomponent binder ...	53
Figure 33: Measured viscosity of WB50 multicomponent binder.....	54



## CHAPTER 1

### 1. INTRODUCTION

Powder Injection Molding (PIM) is the enabling technology which can be used to manufacture complex, precision and net shape components using metal or ceramics [1]. When metal is used in powder-polymer composites, the process is called Metal Injection Molding. Likewise for ceramics, the process is called Ceramic Injection Molding (CIM). CIM which is done at micron level, is often referred as Micro Ceramic Injection Molding ( $\mu$ CIM) [2]. Small parts with complex features are mass produced at low cost using  $\mu$ CIM [3].

Micro-structured components developed from ceramics using  $\mu$ CIM, increase material range available in micro dimensions [4]. With this said, such enhanced products find its applications in various micro-optical or medical applications.

PIM consists of four major steps i.e. feedstock development, injection molding, debinding and sintering. Feedstock is developed by mixing selected powders and multi-component binder system in optimal proportions. This feedstock is then granulated and injection molded to get 100% filled and packed green body. The next step is to get rid of binder from the green body, thus to obtained a porous brown body. The part is then sintered at elevated

temperature to thus obtain near net shape. Sometimes secondary processes are also carried as performed in conventional powder metallurgy [5].

Piezoelectricity can be defined as the ability of certain material to develop electric charge due to external mechanical stress. For bio-imaging application such as ultrasonic transducer, piezoelectric ceramics are been used as they offer a range of dielectric constants, large piezo electric co-efficient and high electromechanical coupling. Lead zirconate titanate,  $\text{Pb}(\text{Zr}_{1-x}\text{Ti}_x)\text{O}_3$  (PZT), has been material of choice for several decades as piezoelectric ceramic [6, 7].

In this particular study, lead zirconate titanate (PZT) mixed homogenous multicomponent binder is used as powder-polymer composite for CIM of microarray. PZT microarrays have been previously established with numerous applications such as nonvolatile memory devices because for their commendable ferroelectric properties; and as sensors in actuators in microelectromechanical systems (MEMS) due to its piezoelectric properties [8-10].

PZT microarrays can be fabricated with different techniques such as rod placement, dice and fill, injection molding, lost mold, tape lamination, fiber processing, co-extrusion and solid free form fabrication. From the above discussed techniques, dice and fill technique is the commercially used technique where a block of fired PZT is micro machined with a series of parallel and perpendicular cuts to form the microarrays[11]. The size of micro pillars is dependent on the accuracy of dicing saw and ability of ceramic to withstand the process. The dicing process itself is time consuming. CIM is relatively faster alternative than this commercially used technique. With CIM, a variety of rod size, shape and spacing can also be obtained [7]. But feedstock development is the crucial step in any CIM process as any defect in its formulation cannot be corrected in subsequent steps of CIM. Thus it is

important for the feedstock to be uniform and homogeneous without any powder-binder particle segregation. Failure to obtain uniform powder concentration due to unsuitable rheological behavior of feedstock will cause to various molding defects such as distortion, cracks or voids. These defects during PIM in turn leads to non-uniform shrinkage or warping in the sintered parts [5, 12].

Therefore, the main goal of this study is to reduce trial and error in feedstock development by using an existing feedstock model to estimate material properties (density, viscosity, specific heat, thermal conductivity and specific volume) and validate simulations performed using estimated properties with PIM experiments. This work was funded by Agency for Defense Development, South Korea and was researched in collaboration with an international university, POSTECH, South Korea.

Various compositions of feedstock was developed and studied with various content of PZT powder and multicomponent binder. **Chapter 2** studies the 45 vol. % PZT-binder composition. Material properties of the feedstock are estimated and Moldex3D simulations are performed. The mold filling behavior, part weight and shrinkage is studied for a flat plate geometry. The results of the simulations are validated using experiments. **Chapter 2** was presented as a conference paper for POWDERMET2017 conference, held in Las Vegas. This work was published in *Advances in Powder Metallurgy & Particulate Materials 2017* and *Powder Injection Molding International* vol. 11 no. 3. This work “Influence of feedstock property estimates and simulations on PIM of PZT” will soon be published as a journal article too.

The understandings from **Chapter 2** were then applied in **Chapter 3**. **Chapter 3** follows the same feedstock development approach but with 52 vol. % PZT powder. In this study,

simulations using estimated feedstock properties for intricate geometry of microarray was successfully validated using experiments. An extensive study on simulations was also conducted in this chapter to understand possible defects in PIM experiments. Research presented in **Chapter 3** is under preparation for submission in “MIM2018: International Conference on Injection Molding of Metals, Ceramics and Carbides” and journal article.

**Appendix B** and **C** reports the study of effect of change in gate location and micro pillar spacing with 3 different microarray geometry. **Appendix D** reports the raw rheology data for powder-polymer composites.

## CHAPTER 2

### 2. INFLUENCE OF FEEDSTOCK PROPERTY ESTIMATES AND MEASUREMENTS ON POWDER INJECTION MOLDING OF LEAD ZIRCONATE TITANATE (PZT)

#### 2.1. INTRODUCTION

Piezoelectric ceramics for transducer applications such as actuators, sensors, capacitors, resonators, and high-power transducers have been widely studied [13, 14]. In order to optimize physical and electromechanical properties of transducer, piezoelectric/polymer composite that consists of active piezoelectric ceramic and passive polymer matrix has been developed [15-18]. Among various piezoelectric ceramic materials, PZT has very high piezoelectric and dielectric properties and is widely used for transducer applications [19]. Various fabrication methods were developed to fabricate piezoelectric/polymer composites such as laser ablation, casting, embossing, micro-pressing, injection molding and fused deposition method. Among these powder injection molding (PIM) is a well-known for high production rate and complex geometries. Even though, there is previous work on PIM of piezoelectric ceramics, the features sizes are higher than hundreds of microns. It is very difficult to produce high aspect ratio fine features of piezoelectric ceramics using PIM. However, injection molding experiments are highly sensitive to

feedstock properties and processing conditions. Mold flow computer simulation of traditional injection molding is frequently used in the process optimization. In order to perform a reliable simulation, extended input data have to be provided. Rheological, PVT, specific heat, thermal conductivity, and density data (in the solid and in the molten state) are some of the material properties required as input for the simulation. Some of the properties like thermal conductivity of the PIM feedstock are difficult to measure and are rare in the literature. In addition, it is very expensive to measure all the required properties. Some attempts have also been made to estimate the feedstock properties from measured binder properties for injection molding of ceramic powders [12, 20].

3D PIM simulation can be used to optimize the injection molding by effectively reducing the design-to-implementation cycle time, identifying key problems before doing the actual fabrication. Among different, mold flow simulation platforms, Moldex3D is a leading CAE product for PIM industry. It can carry out in-depth simulation for widest range of injection molding processes and to optimize product designs and manufacturability [4]. The aim of the current study is to validate the estimated material properties for 3-dimensional mold flow simulations specifically for 45 vol. % PZT feedstock by comparing with the experimental results. Subsequently, the effects of feedstock properties on the mold filling behavior and defect formation were studied using the Moldex3D simulation platform. The results from the present study will provide a quantitative understanding of the influence of estimated feedstock properties on injection molding process.

## 2.2. EXPERIMENTAL MATERIALS AND METHODS

Commercially available PZT was used for feedstock preparation. The morphology of the PZT powder was observed by the scanning electron microscopy (SEM Philips XL30S FEG) and is shown in Figure 1. It can be observed that the fine powders with irregular shape and some amount of agglomeration. Table 1 summarizes the size and density values for PZT powder. A multicomponent binder system consisting of paraffin wax, polypropylene, polyethylene-g-maleic anhydride (L DPE-g-MA), and stearic acid (SA) was used in the current study. Binder system composition details and mixing preparations are provided elsewhere [21].

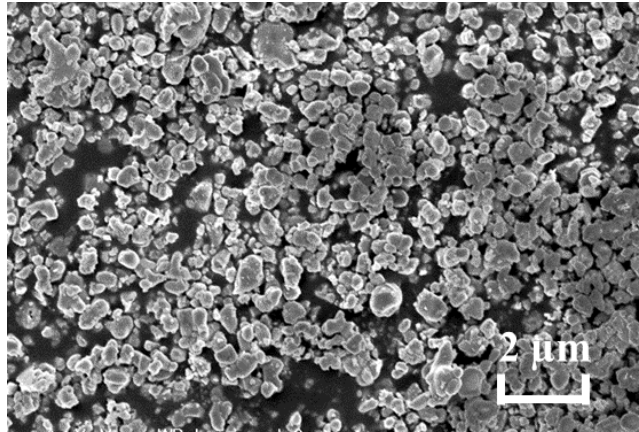


Figure 1: SEM image of PZT powder

**Table 1: PZT powder properties**

Particle size ( $\mu\text{m}$ )			Density ( $10^3 \text{ Kg/m}^3$ )			Dielectric constant
(D <sub>10</sub> )	(D <sub>50</sub> )	(D <sub>90</sub> )	Apparent	Tap	Pycnometer	
0.31	0.52	1.01	1.62	2.54	7.98	3731

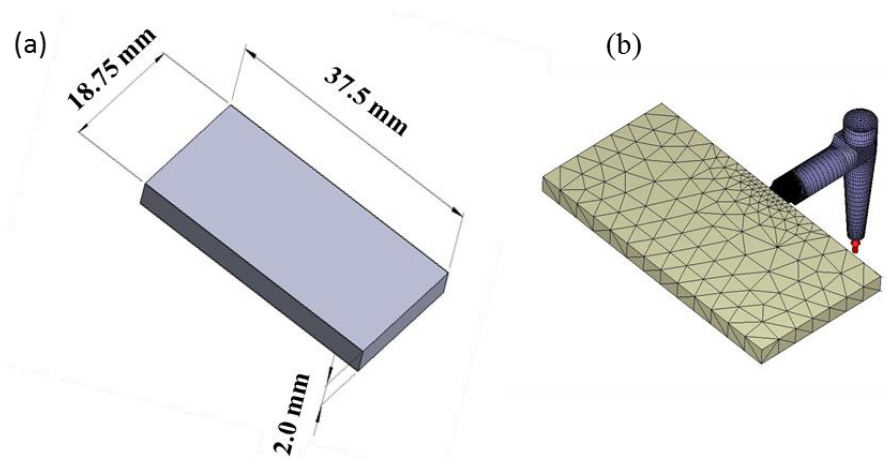
The rheological properties of the binder were measured using a Gottfert Rheograph 2003 capillary rheometer at different shear rates and temperatures. The testing was carried out in accordance with ASTM D3835. The temperatures were between the highest melting

temperature and the lowest degradation temperature of the binder system. Torque rheometry was performed in the Intelli-Torque Plasticorder (Brabender) in order to determine the maximum packing density of the powder-polymer mixture. The Readco Kurimoto continuous processor with twin shaft is used for continuous extrusion of PZT feedstocks. In this process, two K-Tron T-20 twin screw gravimetric feeders were used for to feed the binder and PZT powder, separately. Injection molding was performed on Sodick Plustech TR 30EH injection molding machine. Thermogravimetric analysis (TGA) was performed on the extruded feedstocks using TA- Q500 (TA instruments) thermal system operated under nitrogen flow in the temperature range of 50-600°C with a heating rate of 20 °C/min in order to confirm the powder weight fraction in the feedstock. A K-System II Thermal Conductivity System was used to measure the thermal conductivity of the binder. The testing was carried out in accordance with ASTM D5930. Specific heat measurements were carried out on Perkin Elmer DSC7 equipment in accordance with ASTM E1269. The cooling rate was kept constant of 20°C/minute. A Gnomix PVT apparatus was used to find the PVT relationships of the feedstock materials. The test was carried out in accordance with ASTM D792. Further experimental details will be described elsewhere [20].

PIM experiments were performed using a Sodick HS30ES micro-injection molding machine. PIM experiments were performed at injection molding conditions of 40MPa injection pressure, melt temperature of 433 K, mold temperature of 318 K and injection velocity of 90 mm/s. Moldex3D software was used to perform PIM simulations for the same process conditions as the PIM experiments. The rectangular plate geometry was designed using Solidworks 2016 software and was imported in the Moldex3D R14.0 software and a runner and sprue system. Moldex3D Mesh Designer software was used to



generate mesh with 200,000 mesh elements for the rectangular plate and exported to Moldex3D R14.0. Simulations were conducted for 45 vol. % PZT using estimated material properties. The designed rectangular plate geometry is shown in Figure 2(a) and the meshed plate with runner and sprue are shown in Figure 2(b). Simulations were performed for fill-and-pack conditions.



**Figure 2: Rectangular plate (a) Solidworks part file (b) Meshed with runner gate system in Moldex3D Designer**

## 2.3. RESULTS AND DISCUSSION

### 2.3.1. ESTIMATING PROPERTIES OF POWDER-POLYMER MIXTURES

The experimentally determined binder physical properties were used to estimate properties of PZT powder-polymer mixtures with 45 vol. % using semi empirical scaling rules that are available to estimate material properties [20, 22]. Table 2 to Table 5 summarizes the estimated material properties. In each table, respective measured binder property is listed in bold. Each table contains a footnote with the equations that were used in calculations. Additionally, the viscosity and PVT data required curve fitting to extract constants required for mold filling simulations using Moldex3D software.

An inverse rule-of-mixtures [22] shown in Equation 3 was used to estimate the melt and solid density of the PZT feedstock. PZT sintered body density was provided by Hayshi Chemical Industry. The mass fractions for powder and binder are 0.88 and 0.12, respectively that were calculated using **Equations1-2**. The melt and solid density of 45 vol. % feedstock is shown in Table 2.

**Table 2: Solid and melt densities of feedstocks with 45 vol. % PZT powder**

Powder vol. %	Melt density (kg/m <sup>3</sup> )	Solid density (kg/m <sup>3</sup> )
<b>0 (binder)</b>	<b>727</b>	<b>879</b>
45	3600	4020
<p><i>Eqn1</i> Powder mass fraction <math>X_p = \frac{\Phi_p \rho_p}{\Phi_p \rho_p + \Phi_b \rho_b}</math></p> <p><i>Eqn2</i> Binder mass fraction <math>X_b = \frac{\Phi_b \rho_b}{\Phi_p \rho_p + \Phi_b \rho_b}</math></p> <p><i>Eqn3</i> Inverse rule-of-mixtures <math>\frac{1}{\rho_c} = \frac{X_b}{\rho_b} + \frac{X_p}{\rho_p}</math></p> <p><math>\Phi_p</math> - volume fraction of powder, <math>\Phi_b</math> - volume fraction of binder, <math>\Phi_c</math> - volume fraction of composite, <math>\rho_p</math> - density of powder, <math>\rho_b</math> - density of binder, <math>\rho_c</math> - density of composite</p>		

The specific heat of powder-polymer mixtures has been estimated by different mixing rules [23-27]. In this study, a model that has been successfully applied to mixtures with high volume fraction fillers [24] was used as shown in **Equation 4**. The parameter, A, is a correction factor assumed to be 0.2 for spherical particles. The specific heat values calculated at various temperatures are shown in **Table 3**. In this study, a general rule-of-mixtures model [22] was used as represented in **Equation 5** to estimate the thermal conductivity. The estimated values of thermal conductivity at various temperatures are shown in **Table 3**.

**Table 3: Specific heat capacity and thermal conductivity values at various temperatures for feedstocks with 45 vol. % PZT powder**

Specific heat capacity, $C_p$ (J/kg-K)		
Temperature (K)	Powder volume %	
	0 (Binder)	45
283	2077	632
322	3360	977
352	3840	807
368	4894	1515
377	4639	668
407	3484	680
443	2528	696
Thermal conductivity (W/m·K)		
Temperature (K)	Powder volume %	
	0 (Binder)	45
315	0.2	0.46
336	0.2	0.45
356	0.2	0.45
377	0.2	0.44
397	0.2	0.43
417	0.2	0.42
436	0.2	0.42
$Eqn^4 \text{ Specific heat } C_{p_c} = [C_{p_b}X_b + C_{p_p}X_p] * [1 + A * X_bX_p]$ $Eqn^5 \text{ Thermal conductivity } \lambda_c = \lambda_b\phi_b + \lambda_p\phi_p$		

The specific volume was calculated using the general rule-of-mixtures as shown in **Equation 6** [22]. **Figure 2** shows the comparative plot of specific volumes at 0, 100, and 200 MPa pressure for 45 vol. % PZT powder. Additionally, to perform mold-filling simulations in Moldex3D software, specific volume of the material needs to be represented in terms of fitted constants. There are multiple parameters ( $b_5, b_6, b_9, b_{3m}, b_{4m}, b_{3s}$  and  $b_{4s}, b_{1m}, b_{2m}, b_{1s}$  and  $b_{2s}, b_7$  and  $b_8$ ) related to specific volume are the required input parameters for Moldex3D simulation software. A Dual-domain Tait Equation (**Equation 7, Table 4**) was used to extract these fitted constants using curve fitting for 0, 50, 100, 150, 200 MPa pressure for 45 vol. % PZT powder. The values of these coefficients are summarized in **Table 4**.

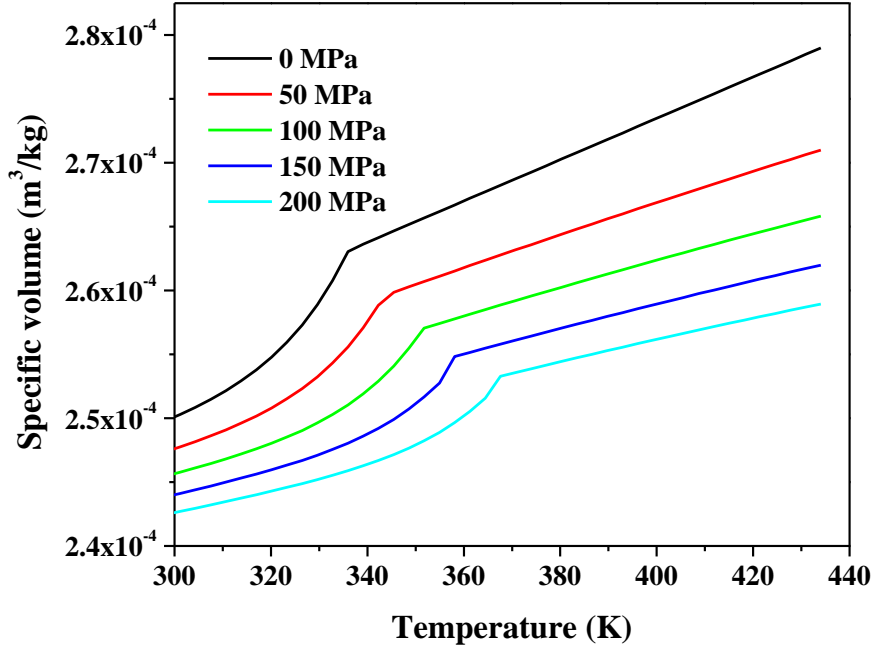


Figure 3: PVT behavior for 0, 100, and 200 MPa pressures for 45 vol. % PZT powder.

Table 4: Dual-domain Tait constants for feedstocks with 45 vol. % PZT powder

dual-domain Tait constants	Powder volume %	
	0 (Binder)	45
$b_5, K$	336	336
$b_6, K/Pa$	$1.5 \times 10^{-7}$	$1.54 \times 10^{-7}$
$b_{1m}, m^3/kg$	$1.3 \times 10^{-3}$	$2.63 \times 10^{-4}$
$b_{2m}, m^3/kg \cdot K$	$1.3 \times 10^{-6}$	$1.13 \times 10^{-7}$
$b_{3m}, Pa$	$1.3 \times 10^8$	$2.24 \times 10^8$
$b_{4m}, K^{-1}$	$6.0 \times 10^{-3}$	$3.04 \times 10^{-4}$
$b_{1s}, m^3/kg$	$1.2 \times 10^{-3}$	$2.52 \times 10^{-4}$
$b_{2s}, m^3/kg \cdot K$	$8.6 \times 10^{-7}$	$1.24 \times 10^{-7}$
$b_{3s}, Pa$	$2.4 \times 10^8$	$5.08 \times 10^8$
$b_{4s}, K^{-1}$	$4.2 \times 10^{-3}$	$1.46 \times 10^{-3}$
$b_7, m^3/kg$	$8.5 \times 10^{-5}$	$1.20 \times 10^{-5}$
$b_8, K^{-1}$	$6.7 \times 10^{-2}$	$9.40 \times 10^{-2}$
$b_9, Pa^{-1}$	$1.4 \times 10^{-8}$	$2.05 \times 10^{-8}$

$$\text{Eqn6} \quad \text{Specific volume } v_c = X_p v_p + v_b(1 - X_f)$$

$$\text{Eqn7} \quad v(T, p) = v_o(T) \left[ 1 - C \ln \left( 1 + \frac{p}{B(T)} \right) + v_t(T, p) \right]$$

$$T > T_i: \quad v_o = b_{1m} + b_{2m}(T - b_5),$$

$$B(T) = b_{3m} e^{[-b_{4m}(T-b_5)]},$$

$$v_t(T, p) = 0$$

$$T < T_i: \quad v_o = b_{1s} + b_{2s}(T - b_5),$$

$$B(T) = b_{3s} e^{[-b_{4s}(T-b_5)]},$$

$$v_t(T, p) = b_7 e^{[b_8(T-b_5)-(b_9p)]}$$

$v(T, p)$  - specific volume at a given temperature and pressure

$v_o$  - specific volume at zero-gauge pressure,  $p$  - pressure,

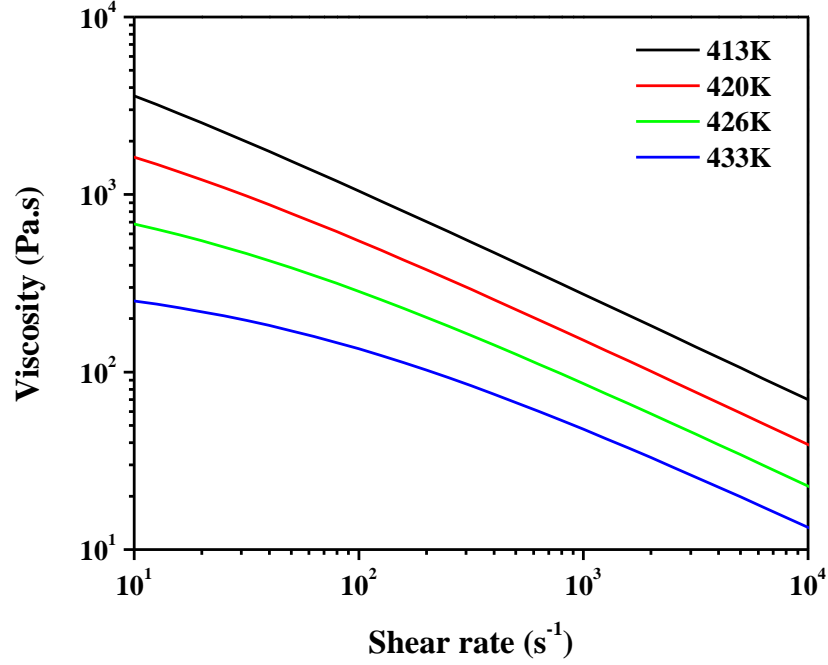
$C$  - constant, 0.0894

$b_{1s}, b_{2s}, b_{3s}, b_{4s}, b_5, b_7, b_8, b_9$  - curve-fitted coefficients

$b_{1m}, b_{2m}, b_{3m}, b_{4m}, b_5, b_6$  - curve-fitted coefficients

A simplified Krieger-Dougherty [28] viscosity model was used to estimate the viscosity values (Equation 8, Table 5). The Cross-WLF model [29] was used to model the viscosity dependence of the powder-polymer mixture on shear rate (Equation 9, Table 5). The temperature dependence of viscosity of PZT powder-polymer mixture [29] was estimated using Equation 10. The values of the coefficients ( $T^*$ ,  $D_1$  and  $A_1$ ,) were extracted by curve-fitting the estimated viscosity for 45 vol. % PZT powder at various shear rates and temperatures. Figure 3 shows the shear-rate dependence of viscosity for feedstocks with 45 vol. % PZT powder at 413, 420, 426 and 433 K. The zero-shear viscosity was estimated from the plateau region at low shear rate while the power law index was obtained from the slope at higher shear rates. The curve-fitted WLF parameters  $n$ ,  $\tau^*$ ,  $D_1$ ,  $T^*$ ,  $A_1$  and  $A_2$  were estimated for four different temperatures (413, 420, 426 and 433 K). The estimated

for  $n$  and  $\tau^*$  for each temperature were then averaged. All the coefficients related to viscosity are summarized in Table 5.



**Figure 4: Comparison of viscosity with shear rate at different temperatures for 45 vol. % PZT powder.**

**Table 5: Cross-WLF constants for feedstocks with 45 vol. % PZT powder**

Cross-WLF constants	Powder volume %	
	0 (Binder)	45
$n$	<b>0.40</b>	0.40
$\tau^*, Pa$	<b>793</b>	15831
$D_1, Pa \cdot s$	<b><math>4.29 \times 10^{23}</math></b>	$1.08 \times 10^{16}$
$T^*, K$	<b>333.00</b>	367.87
$A_1$	<b>78.13</b>	56.59
$A_2, K$	<b>51.60</b>	51.60
<i>Eqn8</i> Viscosity of composite	$\eta_c = \frac{\eta_b}{\left[1 - \frac{\phi_p}{\phi_{max}}\right]^2}$	

$$\text{Eqn9 Melt viscosity } \eta = \frac{\eta_0}{1 + \left(\frac{\eta_0 \gamma}{\tau^*}\right)^{1-n}}$$

$$\text{Eqn10 Zero shear viscosity } \eta_0 = D_1 \exp \left[ -\frac{A_1(T-T^*)}{A_2+(T-T^*)} \right]$$

$\eta_b$  - viscosity of binder,  $\Phi_p$  - volume fraction of powder,  
 $\Phi_{\max}$  - maximum volume fraction,  $\gamma$  - shear rate  
 $\tau^*$  - critical stress level at the transition to shear thinning  
 $n$  - power law index in the high shear rate regime  
 $T$  - temperature,  $T_t$  - volumetric transition temperature  
 $T^*$ ,  $D_1$ ,  $A_1$  - curve-fitted coefficients,  
 $A_2$  - WLF constant, 51.6 K

### 2.3.2. EXPERIMENTAL AND SIMULATIONS RESULTS

The cavity dimensions and process conditions from the experiments were used to perform simulations. Simulations were carried out with estimate and hybrid feedstock properties as mentioned in the table, at different injection velocities and pressure to predict incomplete to complete mold filling behavior of 45 vol. % PZT feedstock. PIM base plates using different injection velocities are shown in Figure 5. At injection velocity of 90 mm/s and packing pressure of 400 kg/cm<sup>2</sup>, a completely filled mold cavity was achieved. The PIM of completely filled 0.45% PZT base plate samples have an average cavity weight of 5.66 g. From Moldex3D simulations the completely filled mold cavity weight is 5.25gm with estimated properties and 5.43 gm with hybrid properties. The error in estimating cavity weight with respect to experiments around 5 to 7 % using estimated and hybrid properties.

**Table 6: Data set used for simulations**

Material parameters	Feedstock properties	
	Estimated	Hybrid
<b>Density</b>	Estimated density	Estimated density
<b>Specific heat</b>	Estimated specific heat	Estimated specific heat
<b>Thermal conductivity</b>	Estimated thermal conductivity	Estimated thermal conductivity
<b>Viscosity</b>	Estimated viscosity	Experimental viscosity
<b>Specific Volume</b>	Estimated specific volume	Estimated specific volume

Table 6 represent the data set used in Moldex3D simulations. To simulate accurate mold filling behavior, viscosity of developed feedstock was measured and used to replace estimated viscosity in hybrid feedstock properties

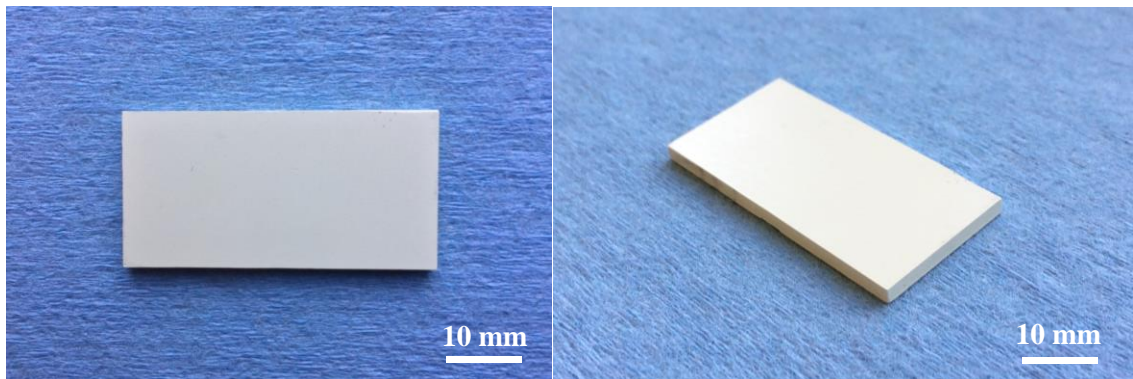


Figure 5: PIM experiment for 45 vol. % PZT rectangular plate with 100% filling at injection velocity 90 mm/s and injection pressure at 40 MPa (a) top view (b) 3D perspective view



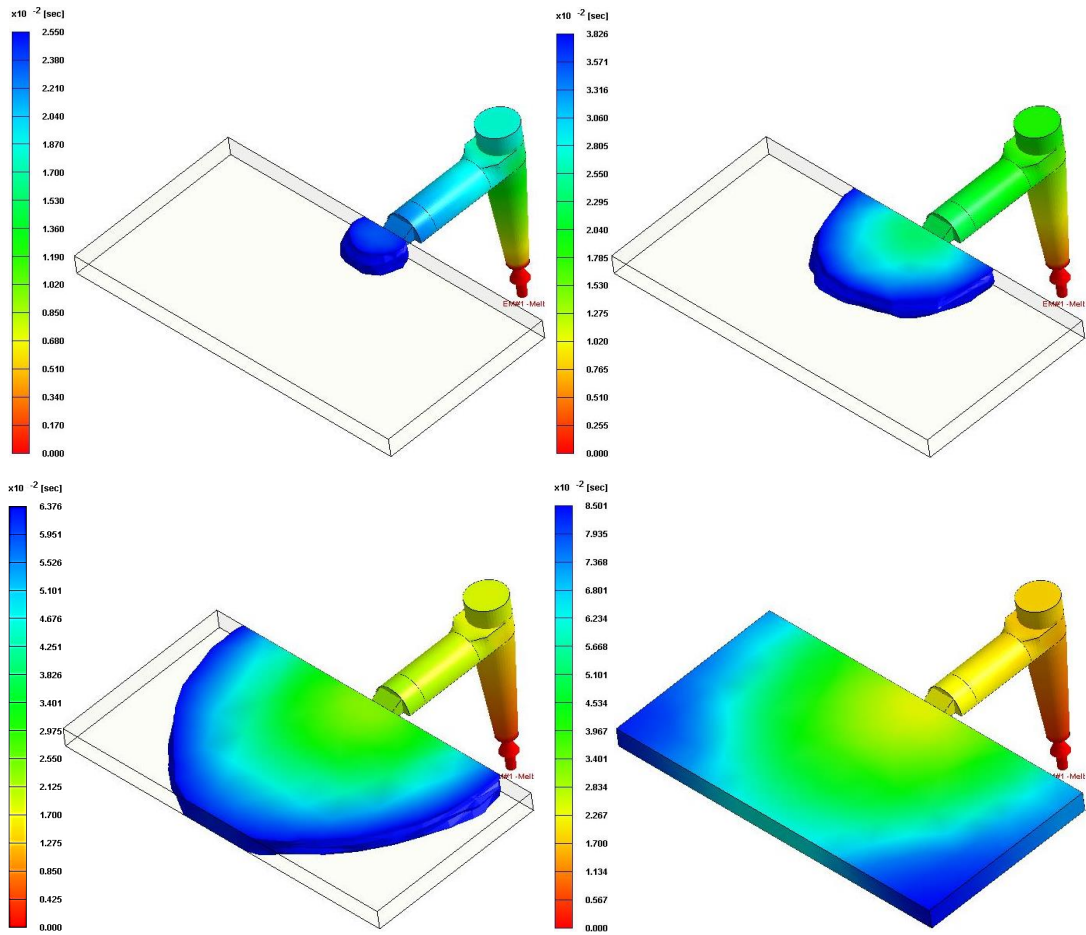


Figure 6: Moldex3D simulation for 0.45% PZT base plate - 100% filled at injection velocity 90 mm/s: (a) 30% filled in 0.025s, (b) 45% filled in 0.038s, (c) 75% filled in 0.064s and (d) 100% filled in 0.085s

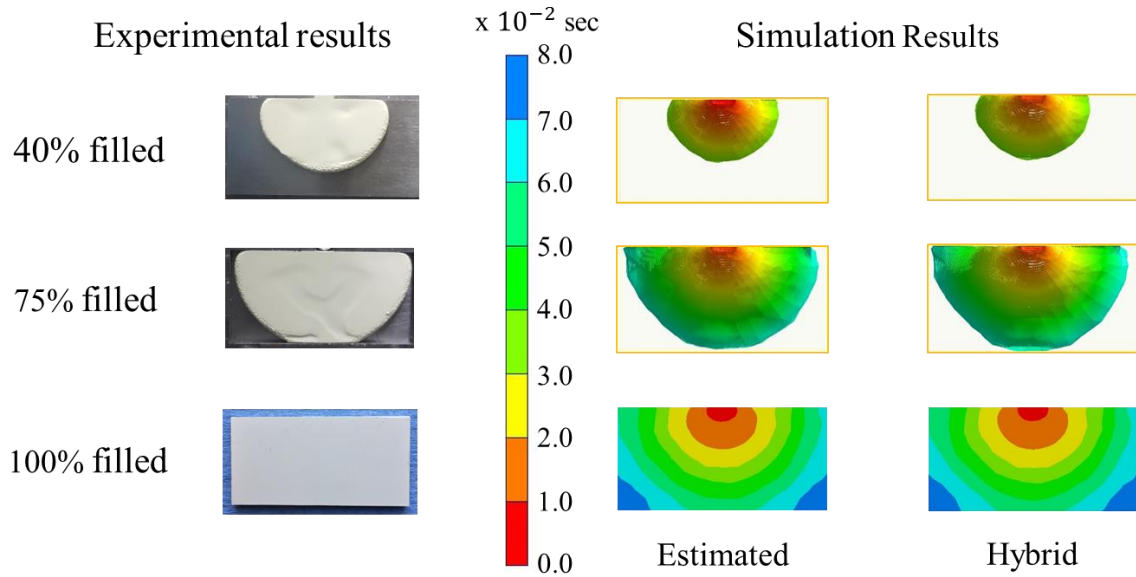


Figure 7: Evolution of simulated flow front for 0.45% PZT base plate compared with experimental results

Figure 6 shows a progressive injection molding behavior inside the rectangular geometry and are comparable to one observed in PIM experiments. Injection molding behavior in a flat plate is further studied in figure 7; it is observed that simulations exactly predict the evolution of mold filling behavior at 40%, 75% and 100%. As seen in experiments, it is expected that the filling flow-front will hit the wall and spread in rest of the cavity. This phenomenon is evidently seen in simulations with hybrid material properties.

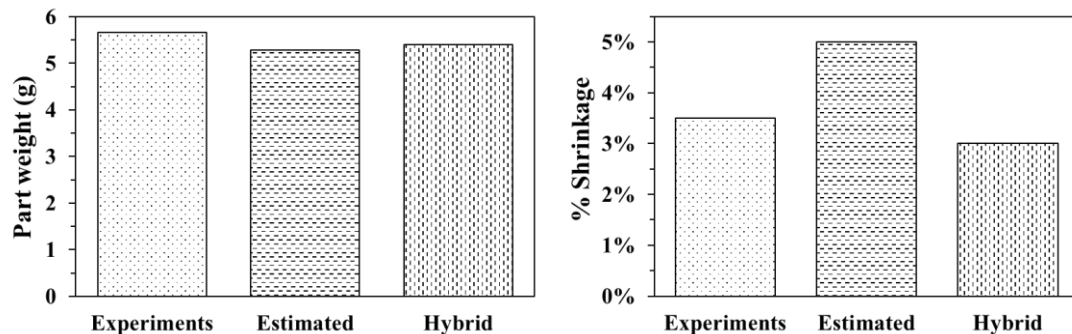


Figure 8: Experiments compared with simulations using estimated and hybrid material properties - (a) Part weight of base plate (b) Volumetric shrinkage (%) of base plate

Table 7: Statistical comparison of experiments compared with simulations using estimated and hybrid material properties (a) relative error in part weight of simulations w.r.t. experiments (b) Volumetric shrinkage (%) of base plate

Cavity Part weight % error	<b>Estimated</b>	<b>Hybrid</b>
	7%	5%

Volumetric shrinkage (%)	<b>Experiments</b>	<b>Estimated</b>	<b>Hybrid</b>
	3.5%	5%	3%

The average volumetric shrinkage for PIM experiment is 3.5% and is 5 % and 3% with Moldex3D simulations.

#### 2.4. SUMMARY

PZT feedstock for 45 vol. % solids loading was successfully formulated and injection molding experiments were performed to get completely molded parts. To perform PIM simulations, physical, thermal, rheological properties and PVT parameters were estimated for 45 vol. % PZT feedstock. Estimated PIM material properties were used as input parameters and PIM simulations were performed using same process conditions as that of PIM experiments process conditions. PIM simulations results indicate that injection molding behavior predicted with PIM simulations is comparable to the molding behavior with experiments. Completely filled base plate weights from PIM experiments and simulation using estimated and hybrid properties were 5.66 gm, 5.25 gm and 5.43 gm respectively. Additionally, volumetric shrinkage predictions with PIM simulations using estimated materials properties (5%) and hybrid material properties (3%) are comparable to PIM experiments (3.5%). Using hybrid material properties to perform PIM simulations can help reduce the number of trial-and-error experiments involved in designing new PIM

feedstocks and PIM process parameters. Furthermore, such an approach can be utilized in selecting component geometry attributes to optimize PIM process.

## CHAPTER 3

### 3. INFLUENCE OF FEEDSTOCK PROPERTY ESTIMATES AND SIMULATIONS ON POWDER INJECTION MOLDING OF LEAD ZIRCONATE TITANATE (PZT) MICROARRAYS

#### 3.1. INTRODUCTION

Lead zirconate titanate (PZT) is most widely and extensively used piezoelectric ceramic. It is used as sensor and actuator for ultrasound probes and various other applications. Commercially, PZT is fabricated using micro machining technique such as dice and fill. A block of fired PZT is micro machined with a series of parallel and perpendicular cuts to form the microarrays[11]. The size of micro pillars is dependent on the accuracy of dicing saw and ability of ceramic to withstand the process. The dicing process itself is time consuming. Powder injection molding(PIM), especially ceramic injection molding (CIM) is a relatively faster alternative than this commercially used technique. With CIM, a variety of rod size, shape and spacing can also be obtained [7]. Any PIM technique consists of the following steps, feedstock formulation, injection molding, debinding and sintering. Feedstock formulation is very important, as it cannot be corrected in any of the subsequent steps. If feedstock formulation for a given geometry is not suitable to PIM, then trial and error technique should be performed to get 100% filled and packed part. In current work,

simulations are performed to study the mold filling behavior of 52 vol. % PZT feedstock with a 3D geometry with micropillar arrays. These simulations are compared to experimental results. In order to perform these simulations, feedstock properties such as viscosity, specific volume, thermal conductivity and specific heat was estimated using semi empirical formulae. A detailed study was also performed on possible defects in PIM of PZT, to avoid any other trial and error in the process.

### 3.2.EXPERIMENTAL MATERIALS AND METHODS

Commercially available lead zirconate titanate (PZT) powder and a wax-polymer binder was used in feedstock development. The binder is composed of paraffin wax, microcrystalline wax, carnauba wax, polypropylene, polyethylene and stearic acid. Maximum solids was determined for PZT polymer composite using torque rheometry which was performed in the Intelli-Torque Plasticorder (Barbender). Feedstock for 52vol% PZT content was developed. Injection molding was performed on Sodick TR30EH injection molding machine. The CAD model was designed in SolidWorks according to the experimental setup. The overall length is 37.50 mm, width 18.75 mm and thickness of 2 mm. The microarray is designed in 3 x 3 configuration with each micro-pillar has length ( $l$ ) of 1 mm and diameter ( $d$ ) of 0.19 mm. The aspect ratio ( $l/d$ ) is 5.263.

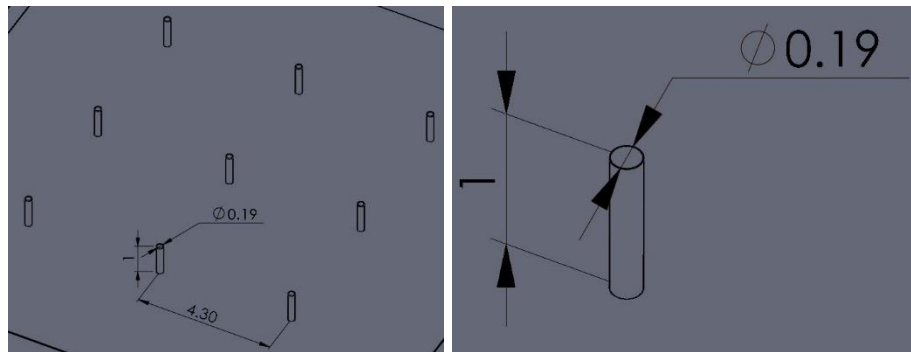
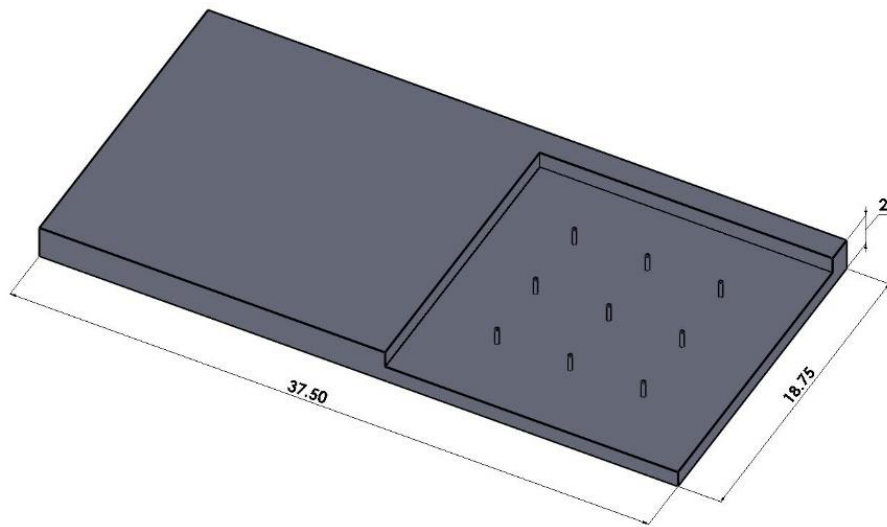


Figure 9: Microarray geometry: SolidWorks part file

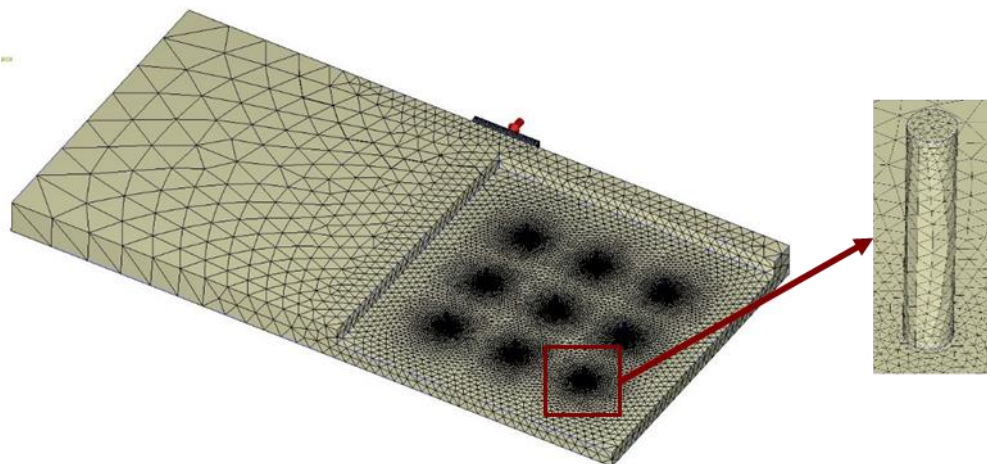


Figure 10: Meshed in Moldex3D designer

The CAD model was then imported in Moldex3D designer as .step file. The model is meshed into 367,868 elements and has mesh volume of 1.11 cc. The PIM process parameters are as shown in table 1. These values were used for PIM experiments and simulations.

**Table 8: Process conditions for powder injection molding**

Process parameter	Values
<b>Mold temperature</b>	60 °C
<b>Melt temperature</b>	160 °C
<b>Ram position</b>	25 mm
<b>Injection velocity</b>	120 mm/s
<b>Packing pressure</b>	40 MPa

Material properties such as specific heat, thermal conductivity, specific volume and viscosity were estimated using semi-empirical formulas and feedstock models. Using these values a material database file for 52vol% PZT was compiled in Moldex3D software. This material file along with process conditions was used for performing simulations.

### 3.3. RESULTS AND DISCUSSION

#### 3.3.1. ESTIMATING MATERIAL PROPERTY

Material properties are estimated for 52 vol. % PZT polymer composite using previous determined binder physical properties. **Table 10 to Table 12** summarizes these estimated properties. Density was estimated as a function of mass fraction. Powder mass fraction was calculated using **Equation (3.10)**

$$X_p = \frac{\phi_p \rho_p}{\phi_p \rho_p + \phi_b \rho_b} \quad (3.1)$$



Binder mass fraction was calculated using **Equation (3.2)**

$$X_b = \frac{\phi_b \rho_b}{\phi_p \rho_p + \phi_b \rho_b} \quad (3.2)$$

Density of powder and binder was measured, and density of composite was estimated with the help of inverse rule of mixtures **Equation (3.3)**.

$$\frac{1}{\rho_c} = \frac{X_b}{\rho_b} + \frac{X_p}{\rho_p} \quad (3.3)$$

**Table 9: Solid and melt densities of feedstock with 52 vol. % PZT powder**

Powder volume %	Melt density (kg/m <sup>3</sup> )	Solid density (kg/m <sup>3</sup> )
0 (binder)	<b>727</b>	<b>879</b>
<b>52</b>	4090	4500

Specific heat and thermal conductivity were estimated as a function of temperature. The specific heat of PZT powder-polymer composite (**Equation (3.4)**) was estimated using specific heat and mass fraction of individual PZT and binder

$$C_{p_c} = [C_{p_b} X_b + C_{p_p} X_p] * [1 + A * X_b X_p] \quad (3.4)$$

The specific heat for 52 vol. % PZT polymer composite for a range of temperature from 283 K to 443 K is as shown in **Table 10**. The thermal conductivity of the composite (**Equation (3.5)**) was estimated using thermal conductivity and volume fraction of PZT powder and binder

$$\lambda_c = \lambda_b \phi_b + \lambda_p \phi_p \quad (3.5)$$

**Table 10: Specific heat capacity and thermal conductivity values at various temperatures for feedstock with 52 vol. % PZT powder**

Specific heat capacity, $C_p$ (J/kg-K)		
Temperature (K)	Powder vol %	
	0 (Binder)	52
283	2077	585
322	3360	853
352	3840	721
368	4894	1272
377	4639	613
407	3484	623
443	2528	635

Thermal conductivity (W/m·K)		
Temperature (K)	Powder vol %	
	0 (Binder)	52
315	0.2	0.53
336	0.2	0.52
356	0.2	0.51
377	0.2	0.50
397	0.2	0.49
417	0.2	0.49
436	0.2	0.48

Specific volume was estimated as a function of temperature and pressure. Using rule of mixtures (**Equation (3.6)**) specific volume for 52 vol% PZT feedstock was estimated from pressure 0 to 200 MPa and temperature 10-300°C.

$$v_c = X_p v_p + v_b(1 - X_f) \quad (3.6)$$

Dual-domain Tait model (**Equation (3.7)**) was used to extract constant from curve fitting of specific volume as shown in **Table 11**.

$$v(T, p) = v_o(T) \left[ 1 - c \ln \left( 1 + \frac{p}{B(T)} \right) + v_t(T, p) \right] \quad (3.7)$$

For  $T > T_t$ ,

$$v_o = b_{1m} + b_{2m}(T - b_5)$$

$$B(T) = b_{3m}e^{[-b_{4m}(T-b_5)]}$$

$$v_t(T, p) = 0$$

For  $T < T_i$ ,

$$v_o = b_{1s} + b_{2s}(T - b_5),$$

$$B(T) = b_{3s}e^{[-b_{4s}(T-b_5)]},$$

$$v_t(T, p) = b_7e^{[b_8(T-b_5)-(b_9p)]}$$

**Table 11: Dual-domain Tait constants for binder and 52vol% PZT feedstock**

Dual-domain Tait constants	Powder vol %	
	0 (Binder)	52
$b_5, K$	336	335
$b_6, K/Pa$	$1.5 \times 10^{-7}$	$1.17 \times 10^{-7}$
$b_{1m}, m^3/kg$	$1.3 \times 10^{-3}$	$2.3 \times 10^{-4}$
$b_{2m}, m^3/kg \cdot K$	$1.3 \times 10^{-6}$	$1.26 \times 10^{-7}$
$b_{3m}, Pa$	$1.3 \times 10^8$	$7.34 \times 10^8$
$b_{4m}, K^{-1}$	$6.0 \times 10^{-3}$	$5.0 \times 10^{-4}$
$b_{1s}, m^3/kg$	$1.2 \times 10^{-3}$	$2.28 \times 10^{-4}$
$b_{2s}, m^3/kg \cdot K$	$8.6 \times 10^{-7}$	$1.45 \times 10^{-7}$
$b_{3s}, Pa$	$2.4 \times 10^8$	$2.37 \times 10^8$
$b_{4s}, K^{-1}$	$4.2 \times 10^{-3}$	$1.9 \times 10^{-3}$
$b_7, m^3/kg$	$8.5 \times 10^{-5}$	$5 \times 10^{-6}$
$b_8, K^{-1}$	$6.7 \times 10^{-2}$	$1.8 \times 10^{-1}$
$b_9, Pa^{-1}$	$1.4 \times 10^{-8}$	$2 \times 10^{-8}$

Viscosity was estimated as a function of temperature and shear rate. Viscosity of composite was estimated using simplified Krieger Dougherty model as shown in **Equation (3.8)** [30].

$$\eta_c = \frac{\eta_b}{\left[1 - \frac{\phi_p}{\phi_{max}}\right]^2} \quad (3.8)$$

The Cross-WLF model was used to find the curve fitting constants (**Table 12**) which are required for Moldex3D simulations. Melt viscosity was calculated using **Equation (3.9)**

$$\eta = \frac{\eta_0}{1 + \left(\frac{\eta_0 \dot{\gamma}}{\tau^*}\right)^{1-n}} \quad (3.9)$$

Zero shear viscosity was estimated using **Equation (3.10)**

$$\eta_0 = D_1 \exp \left[ -\frac{A_1(T - T^*)}{A_2 + (T - T^*)} \right] \quad (3.10)$$

**Table 12: Viscosity constants**

Cross-WLF constants	Powder vol %	
	0 (Binder)	52
<i>n</i>	0.40	0.40
<i>τ*</i> , Pa	793	74145
<i>D<sub>1</sub></i> , Pa·s	4.29 x 10 <sup>23</sup>	2.28 x 10 <sup>16</sup>
<i>T*</i> , K	333.00	372.08
<i>A<sub>1</sub></i>	78.13	52.65
<i>A<sub>2</sub></i> , K	51.60	51.60

### 3.3.2. EXPERIMENTS AND SIMULATIONS

Injection molding experiment listed in table 1 was performed with injection velocity of 120 mm/s and packing pressure of 40 MPa and a melt temperature of 160°C with PZT feedstock. The experiments resulted in 100% filled parts with well-defined micro pillars.



Figure 11: Sintered Microarray part

Using feedstock material properties constants from **Table 10 to Table 12**, material database file was created in Moldex3D software. In order to check the effectiveness of PIM simulations in predicting mold filling behavior, simulations were then performed on the meshed part file **Figure 10** using material database file, and process conditions from experiments. The simulations successfully confirmed the mold filling behavior with 100% filled microarray. In simulations, during mold filling it is observed that the base plate is filled completely in x-y direction and when the melt front hits end of fill, the material is filled in microarray pillars along the z direction.

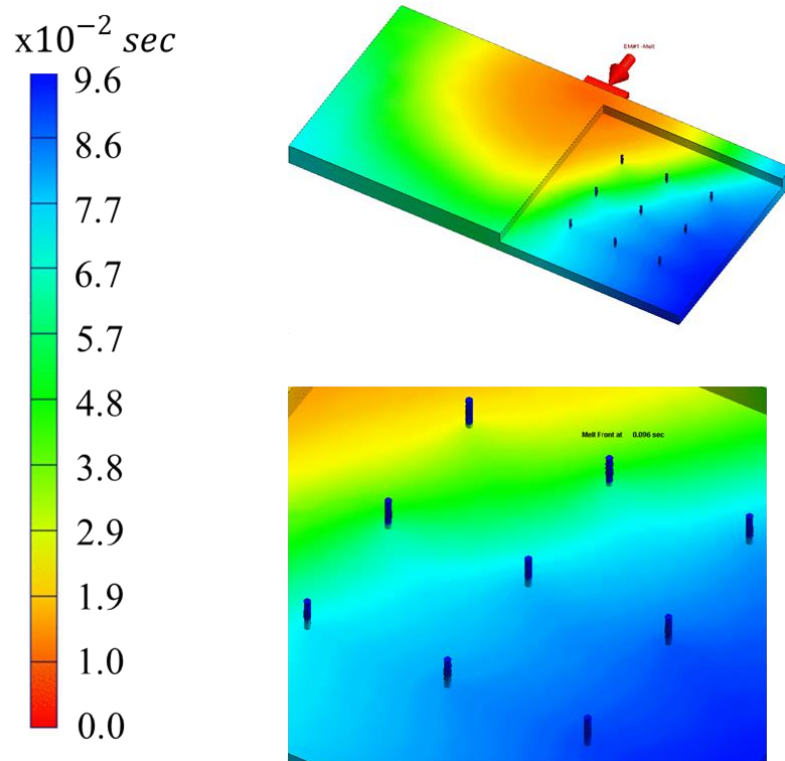


Figure 12: Mold filling behavior in microarray

Table 13: Comparison of part weight with experiments and simulations

<b>Green body - Part weight</b>	
Experiments	Simulations
4.02 gm	<b>4.62 gm</b>

Table 14: Comparison of linear shrinkage in experiments and simulations

<b>Linear Shrinkage</b>	
Experiments	Simulations
1.33%	<b>1.38%</b>

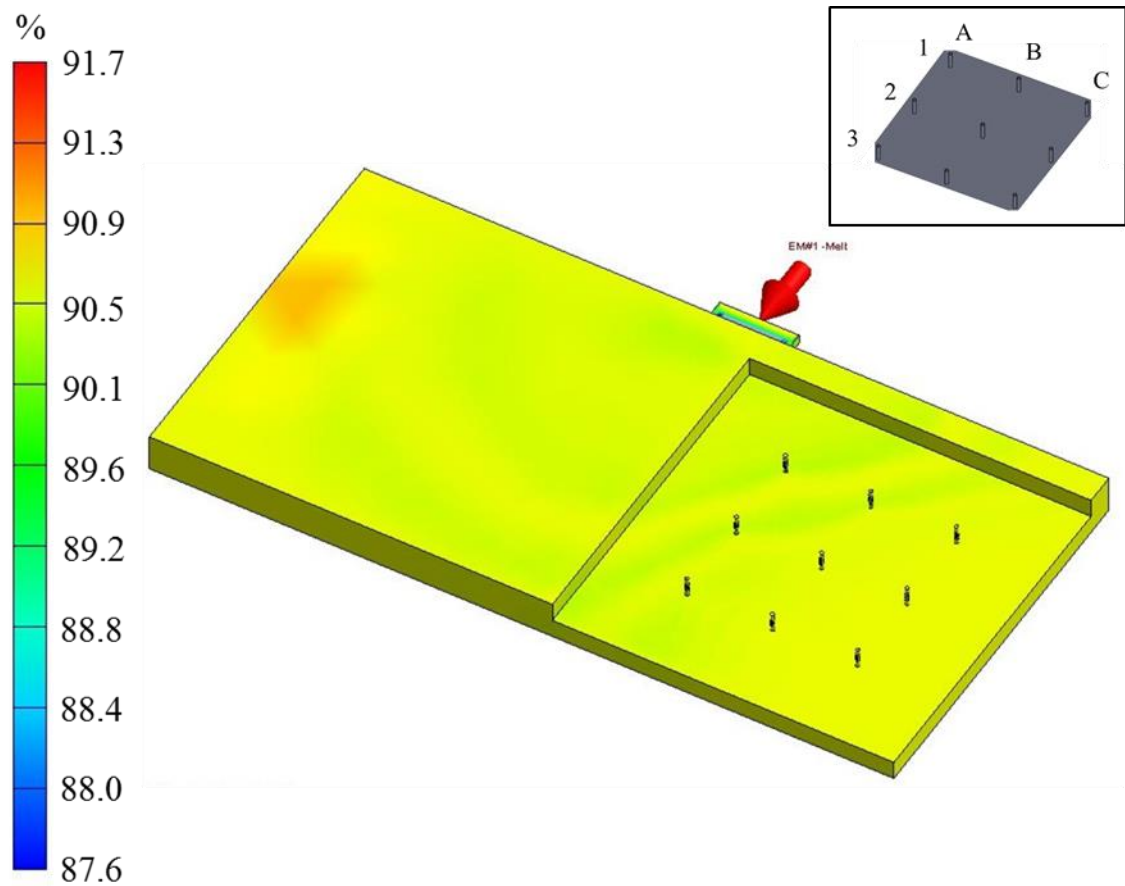


Figure 13: Powder concentration of filled and packed microarray

Powder concentration in the feedstock is 90.06%. During the injection molding simulations it is observed that the powder concentration varies from 87.6% to 91.7%. As seen in figure 5, powder concentration varies with the flow front, with green, yellow and red patched indicating variation in powder concentration. The overall powder concentration looks uniform throughout the surface.

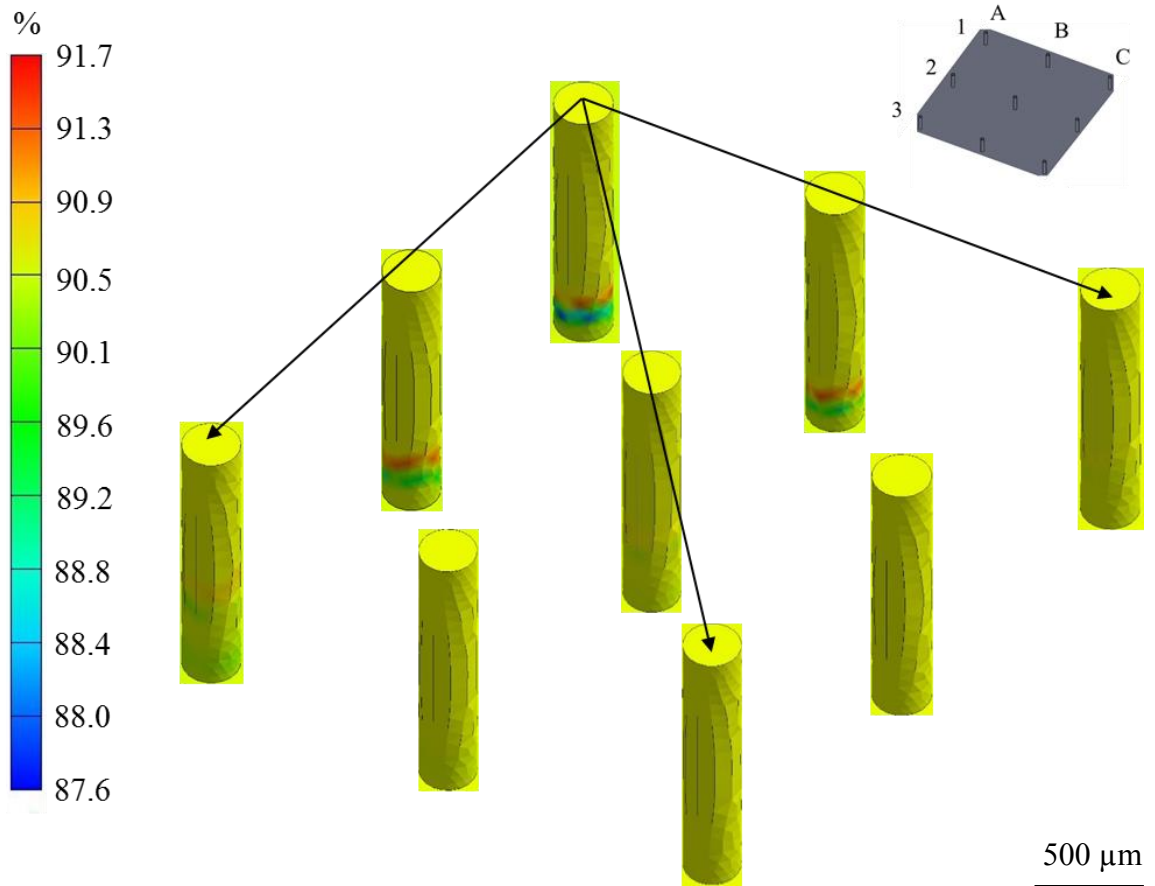


Figure 14: Powder concentration within individual micro-pillars

When the individual micro pillars were closely examined, a lower powder concentration was observed at the bottom of micro pillars as shown in **Figure 15**. A trend was observed in the powder concentration within micro pillars which can be seen in **Figure 14**. **Figure 14** represents the powder concentration in each micro pillar and it can be observed that as you move away from the gate location, the powder concentration becomes more uniform. It can also be implied that micro pillar closest to the gate location has highest amount of variation in powder concentration and the micro pillar farthest from the gate location has least amount of variation.



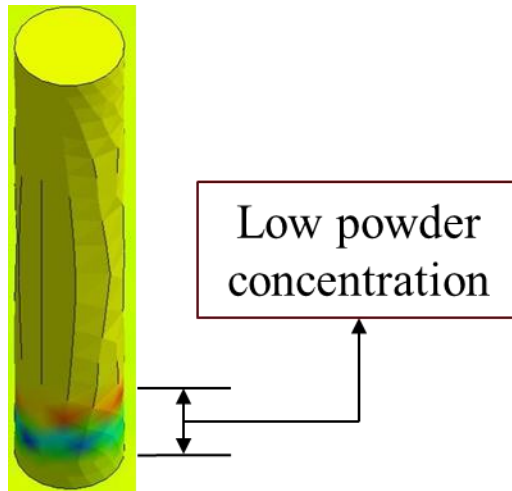


Figure 15: Powder concentration of micro-pillar at location A1

The defect of broken micro pillar during sintering, observed in **Figure 19**, can be attributed to the variation in powder concentration seen during simulations. As the powder concentration at the bottom of micro pillar is less, it will lead to non-uniform shrinkage within the micro-pillar during debinding and sintering of green body. It will result in neck formation in the region of low powder concentration and thus more susceptible to failure.

More detailed study was performed to reason the variation of powder concentration. In simulation, a cross section was taken at the region of low powder concentration (1.08 mm from bottom of base plate) to observe temperature distribution in the microarray configuration during filling. This temperature during mold filling behavior is represented in . It was observed that the temperature during filling varies with the location of micro pillar from the gate location. The micro pillar closest to the gate location had the lowest filling temperature. And the micro pillar farthest away from the gate location had the highest filling temperature.

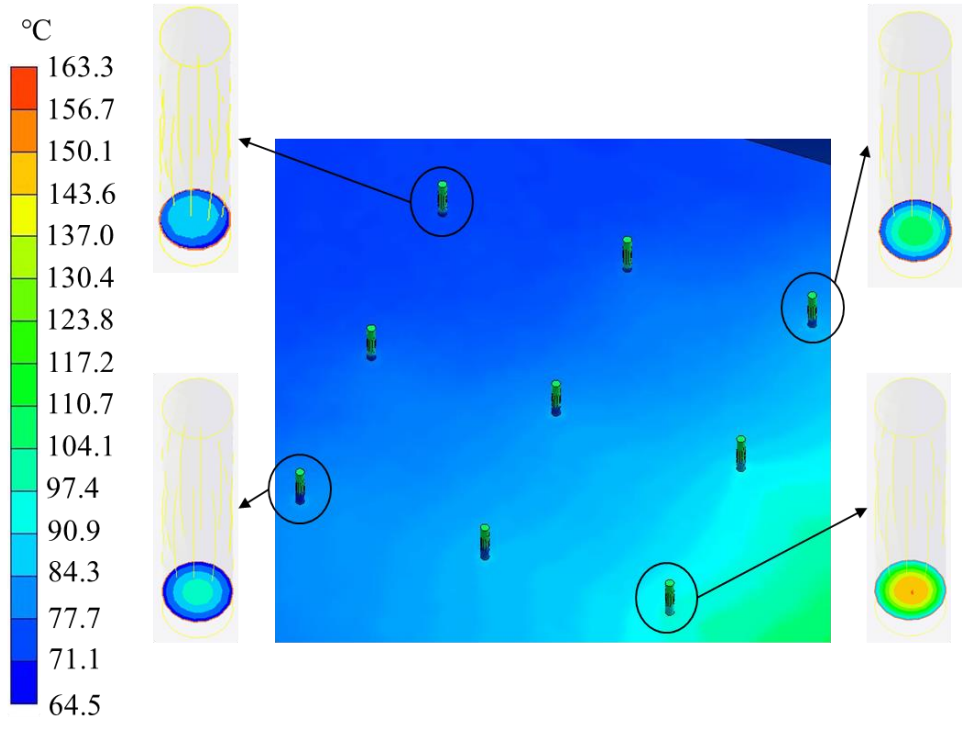


Figure 16: Temperature during filling at bottom of micro-pillar

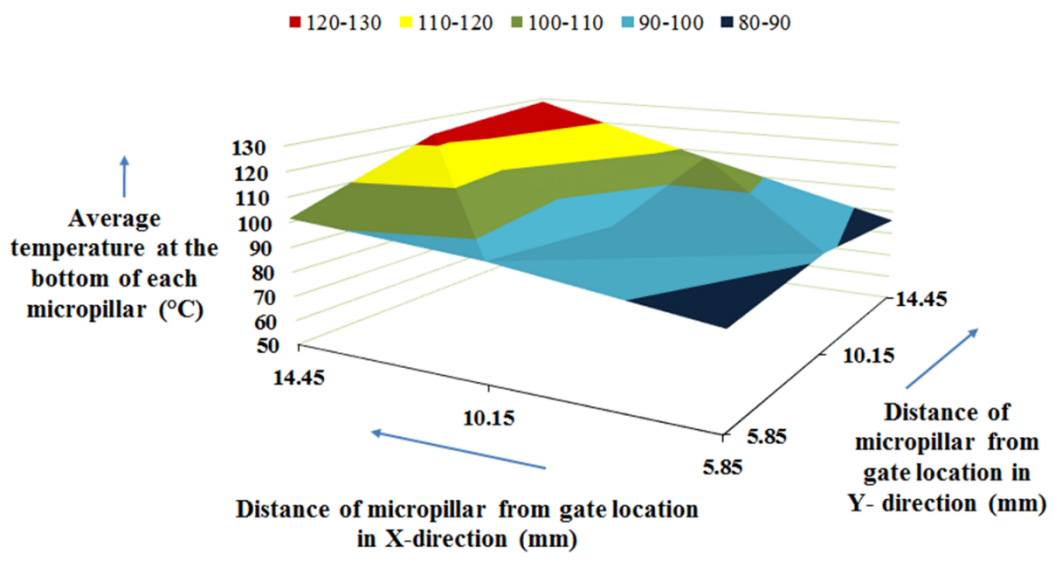


Figure 17: 3D plot of temperature distribution within micro-pillar with respect to its distance from gate location

To further understand this phenomenon, mold filling temperature distribution within a micro pillar was 3D plotted against its x and y distance from the gate location as shown in **Figure 17**. The graph observed is an inclined 3D surface, with increase in x and y distance, the temperature distribution within the micro pillar significantly increases.

When the powder concentration was investigated at the same cross section, a similar 3D graph was plotted with powder concentration % on Z-axis as shown in **Figure 18**.

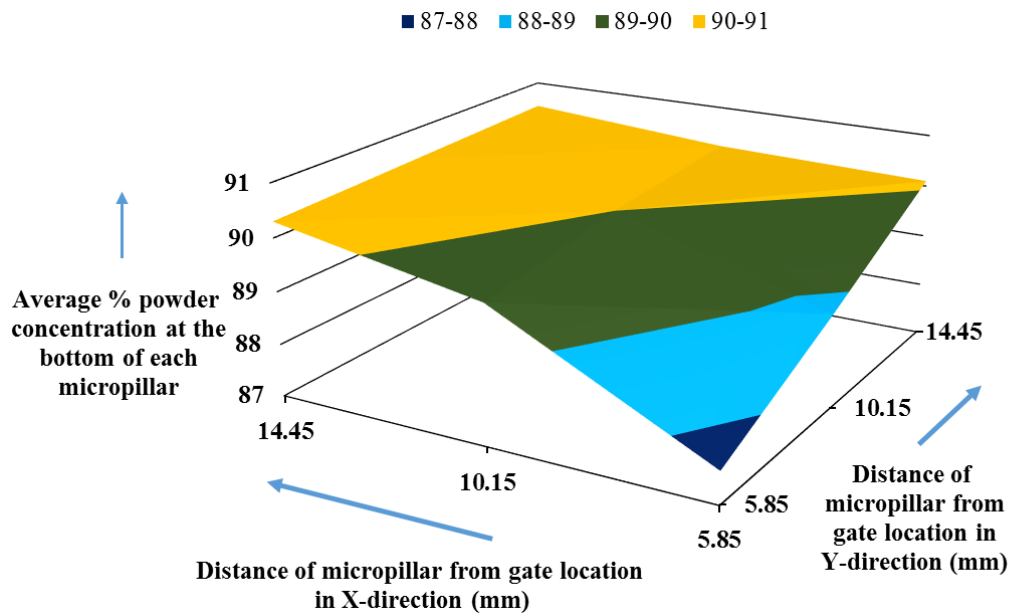


Figure 18: 3D plot of % powder concentration with respect to its distance from gate location

The powder concentration of the PZT feedstock is 90.06%. The micro pillars with filling temperature range from 80 to 90°C have powder concentration of 87 to 88%; 90 to 100°C have powder concentration of 88 to 90% and 100 to 130°C have powder concentration of 90 to 91%.



Figure 19: Broken micro pillars after sintering

From these studies it can be said that, powder concentration is attributed to the mold filling temperature. Lower the mold filling temperature with respect to average filling temperature, lower is the powder concentration. Similarly, a higher filling temperature will lead to more uniform powder concentration. This non-uniform powder concentration will cause to various molding defects such as distortion, cracks or voids. These defects during PIM in turn leads to non-uniform shrinkage or warping in the sintered parts [5, 12]

### 3.4. SUMMARY

PZT feedstock for 52 vol. % solids loading was successfully formulated and injection molding experiments were performed to get completely molded parts. To perform PIM simulations, physical, thermal, rheological properties and PVT parameters were estimated for 52 vol. % PZT feedstock. Estimated PIM material properties were used as input parameters and PIM simulations were performed using same process conditions as that of PIM experiments process conditions. PIM simulations results indicate that injection molding behavior predicted with PIM simulations is comparable to the molding behavior with experiments. Completely filled microarray parts from PIM experiments and simulation using estimated were 5.26 gm and 4.62 gm respectively. Additionally, linear shrinkage predictions with PIM simulations using estimated materials properties (1.38%) is comparable to PIM experiments (1.33%). Using simulations, defects and non-uniform shrinkage during sintering is be predicted by the knowledge of powder concentration and filling temperature of each micro-pillar.

## CONCLUSIONS

With the use of above discussed feedstock model, the goal of reducing trial and errors in developing feedstock for PZT is successfully achieved. Furthermore, simulations can be used as a platform to predict and understanding mold flowing behavior. The results of experiments were in good compliance in with simulations.

- Feedstock properties estimated: PZT 45 vol. % and 52 vol.

(density, thermal conductivity, specific heat viscosity and specific volume)

- Estimated PZT feedstock properties can be used to perform PIM simulations
- Simulations can predict mold filling behavior, part weight and shrinkage

Hence, simulations should be used as a starting point for PIM experiments. Understanding of powder concentration and its correlation to filling temperature is an indicator of possible defects in during actual experiments.

- Sintering defect can be related to powder concentration and temperature distribution
- But exact broken pillar location cannot be predicted

Hence, secondary goal of thesis is also met by predicting possible defects. Thus this research serve as a complete guideline to perform PIM for PZT from feedstock development to net-shape part.

## FUTURE WORK

In this entire study, the simulations were based on estimated material properties except in **Chapter 2**, where hybrid material properties were also used. Such as approach can now be used in simulations using measured material properties based on micro pillar array and understand its proximity with experiments.

Experiments can now be conducted to study effect of change in microarray spacing and gate location. Simulations results are discussed in **Appendix A, B and C**.

Another study can be conducted, is on the debinding and sintering behavior of the PZT ceramic. As during sintering, ceramics usually shrink more than 15%, the knowledge of this behavior will help in designing complex geometries from PZT.

The microarray can further be tested for its dielectric constants, piezoelectric co-efficients and electromechanical coupling. These tested values can then be compared with literature. If a subsequent increase in these piezoelectric properties is observed, then this geometry can be utilized in developing sensors and actuator for ultrasound transducer.

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## APPENDIX

### (A) CAD models and process conditions for simulations

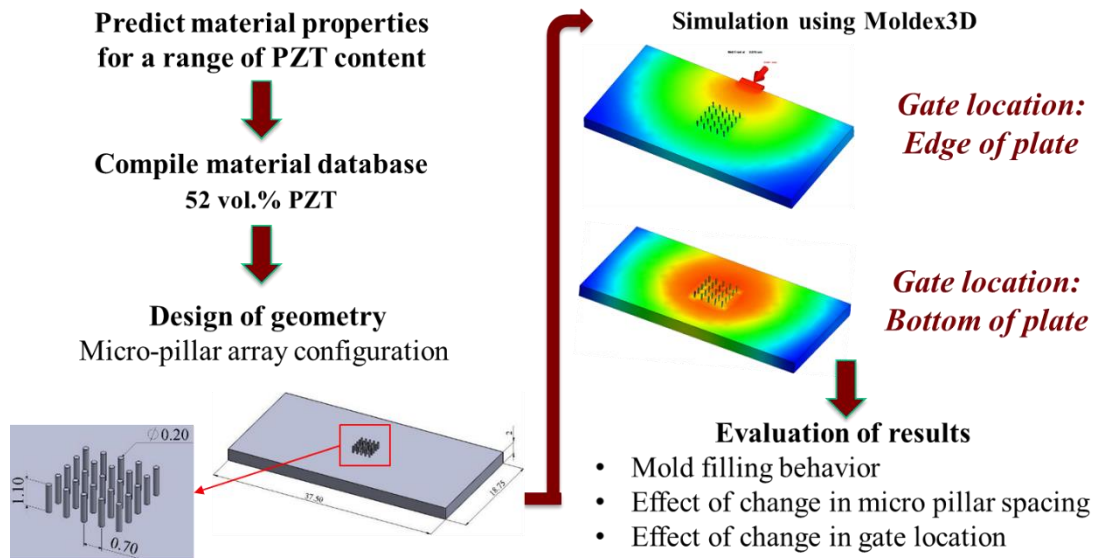


Figure 20: Flow chart for simulations

Figure 20 represents the flow chart used in study of micro-pillar array geometry. Material properties such as density, specific heat, thermal conductivity, viscosity and specific volume were estimated using semi-empirical models. Using the estimated material properties, constants were extracted for simulations in Moldex3D. Microarray geometry was designed for a balanced flow PIM. These geometries were then studied for mold filling behavior, effect of change in microarray spacing and effect of change in gate location.

Using SolidWorks, three different microarray geometries were designed. Each geometry has a unique microarray spacing as shown in figure 21. The base plate geometry and aspect

ratio of the micro-pillar is kept constant in all three designs which is evident in figure 21 (a), (b) and (c).

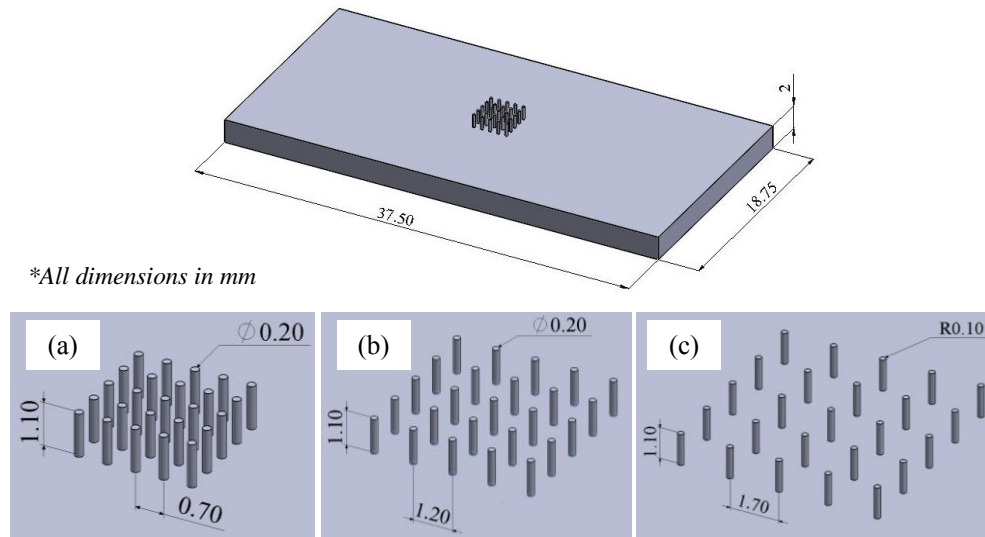


Figure 21: Microarray geometry (CAD model) with inter-pillar spacing (a) 0.7 mm (b) 1.2 mm (c) 1.7 mm

Each micro-pillar has diameter of 200  $\mu\text{m}$  and a height of 1100  $\mu\text{m}$  with inter-pillar spacing of 700  $\mu\text{m}$ , 1200  $\mu\text{m}$  and 1700  $\mu\text{m}$ . These CAD model were then converted to .STEP file format for meshing them in Moldex3D software. During meshing, two different gate locations were used, namely, edge gate and bottom gate. Figure 22 represents the mesh file of microarray geometry with bottom gate location.

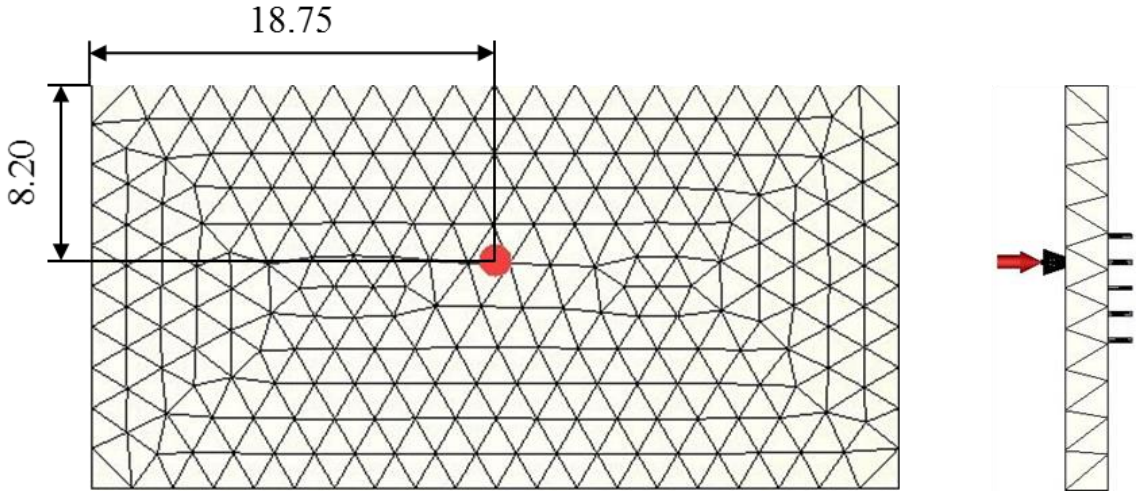


Figure 22: Bottom gate location on the mesh file (Moldex3D)

The bottom gate is purposefully offset from the face center of plate so as to avoid hesitation during mold filling for microarray geometry.

Table 15: PIM process conditions

Process Parameters	Values
Mold temperature, °C	45
Melt temperature, °C	160
Ram position, mm	25
Injection Velocity, mm/s	90
Packing pressure 1, MPa for 8s	40
Packing pressure 2, MPa for 4 s	30

The simulations were setup using the process conditions shown in Table 8.

(B) Effect of change in microarray spacing

1. Mold filling behavior

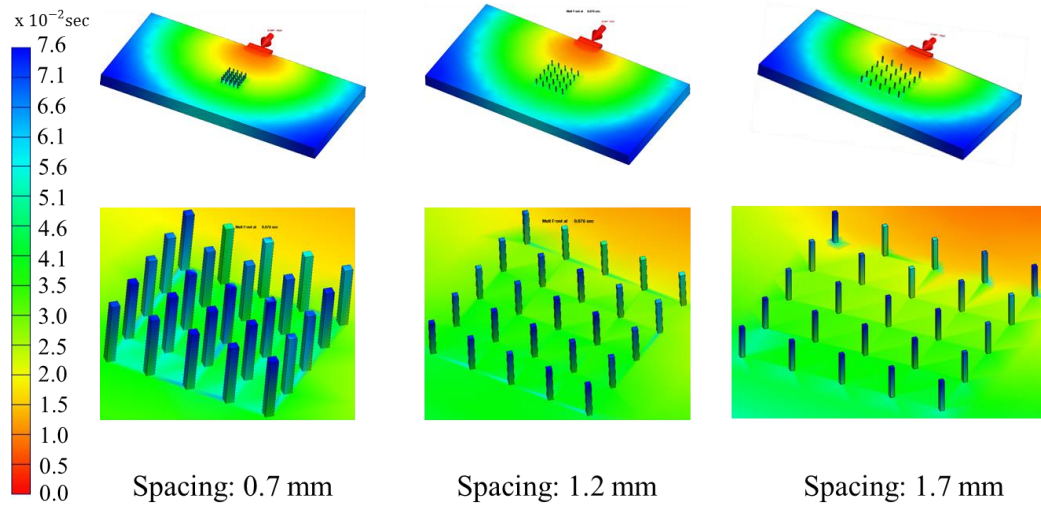


Figure 23: Mold filling behavior for change in microarray spacing

The effect of change in microarray spacing on mold filling behavior is represented in figure 23. It is observed that all the micro pillars are completely filled having part weight of 5.88 gm. Although the fill time is same, it is observed that there is a significant difference in mold filling pattern for each microarray configuration. From simulations, one can conclude that when the microarray spacing is narrow, the flow front is unbalanced with some micro-pillars getting filled faster than the others. But as you increase the microarray spacing, the mold filling behavior becomes more uniform, with number of pillars filling together increases.

## 2. Air traps

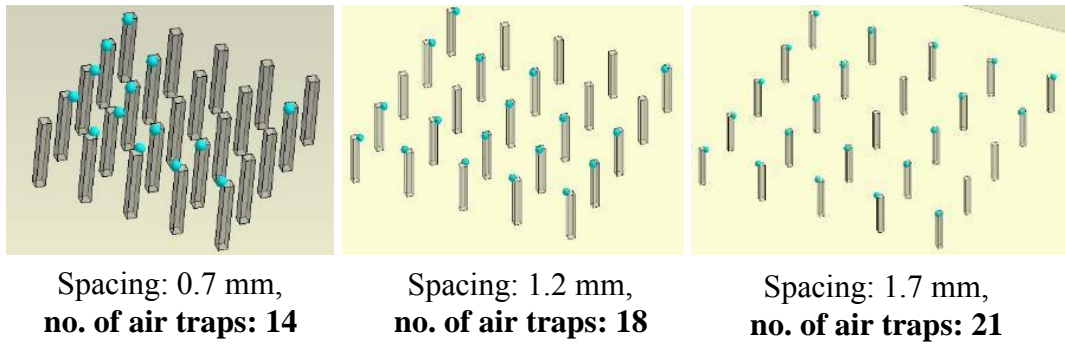


Figure 24: Air traps for change in microarray spacing

## 3. Powder concentration

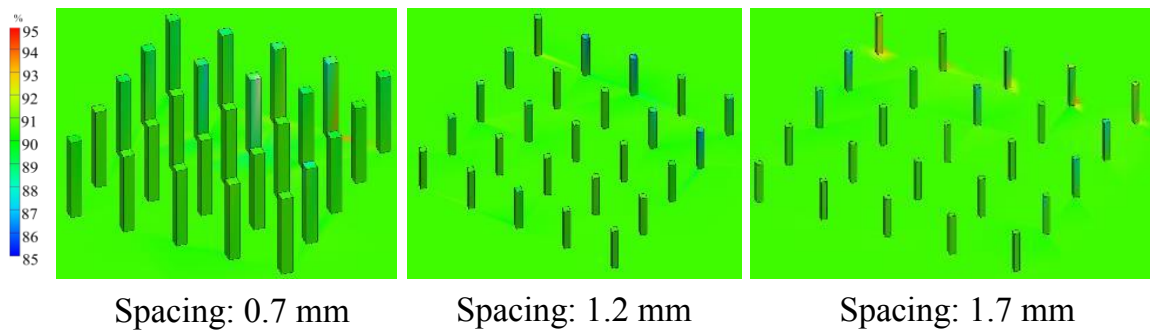


Figure 25: Powder concentration for change in microarray spacing



(C) Effect of change in gate location

1. Mold filling behavior

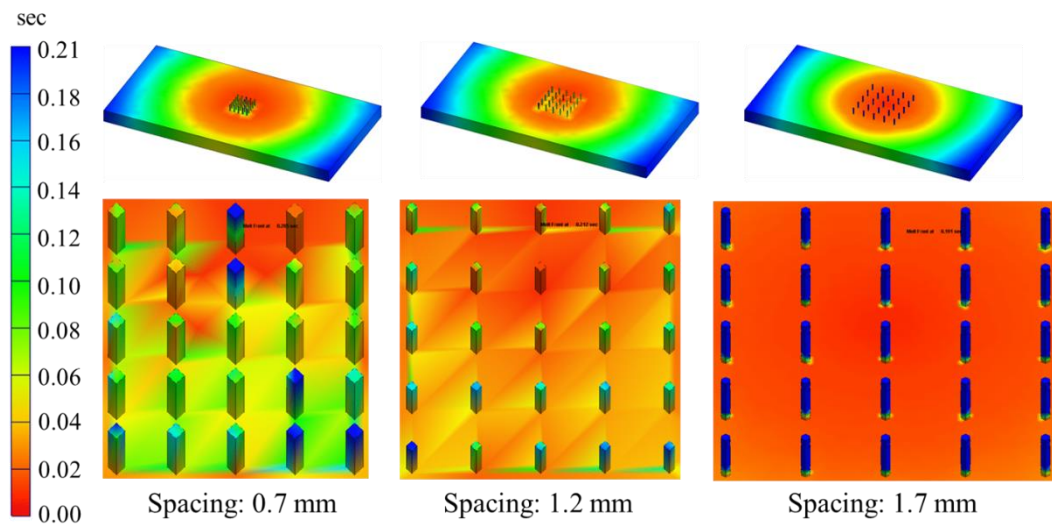


Figure 26: Mold filling behavior for change in gate location

2. Air traps

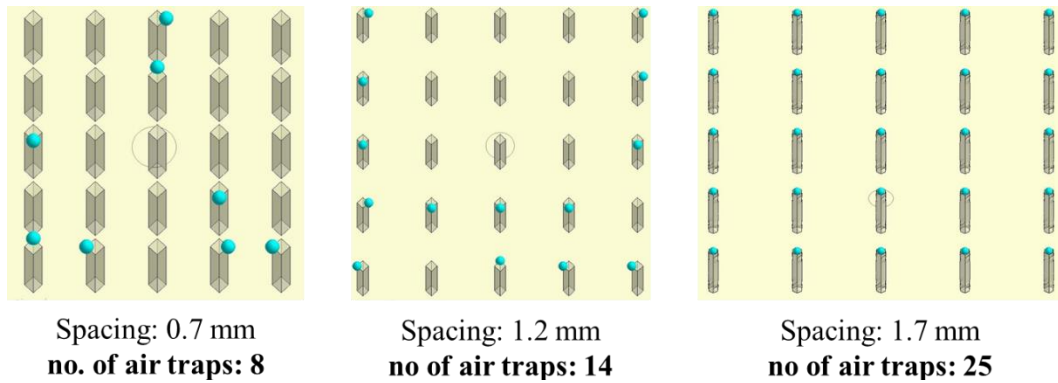


Figure 27: Air traps for change in gate location

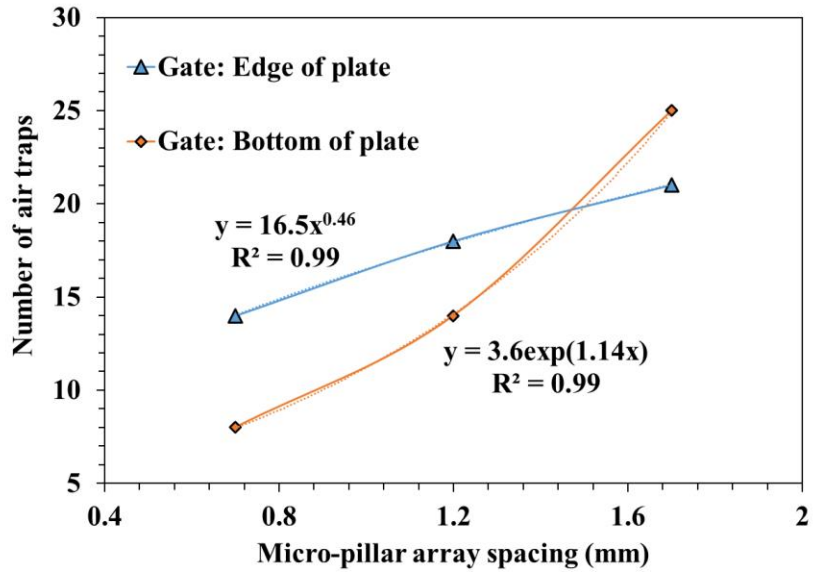


Figure 28: Comparison of air traps for different gate location

### 3. Powder concentration

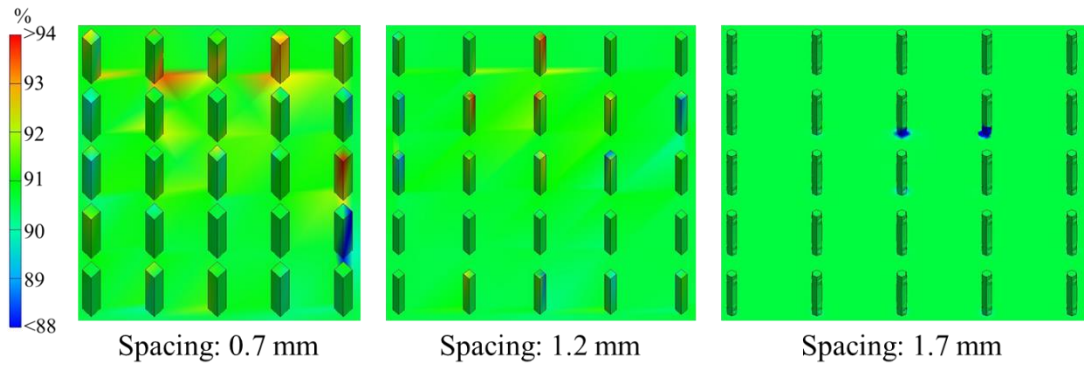


Figure 29: Powder concentration for change in gate location

#### 4. Shear stress

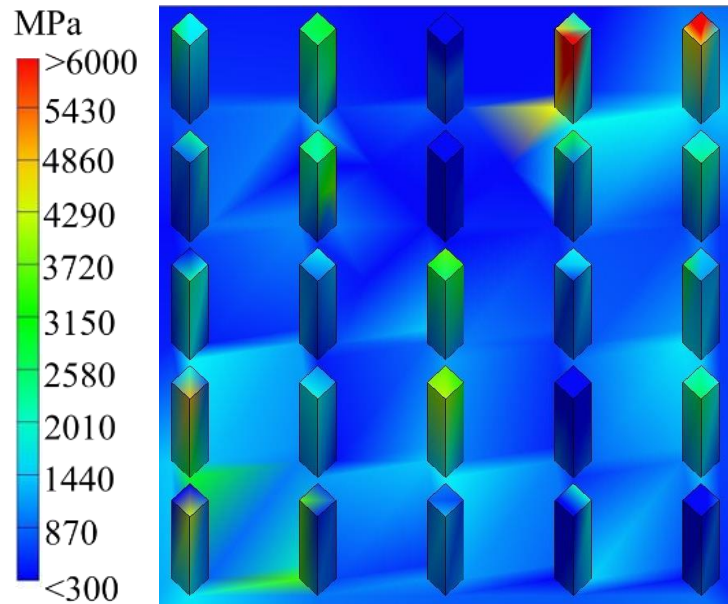


Figure 30: Shear stress for 0.7 mm microarray spacing with bottom gate

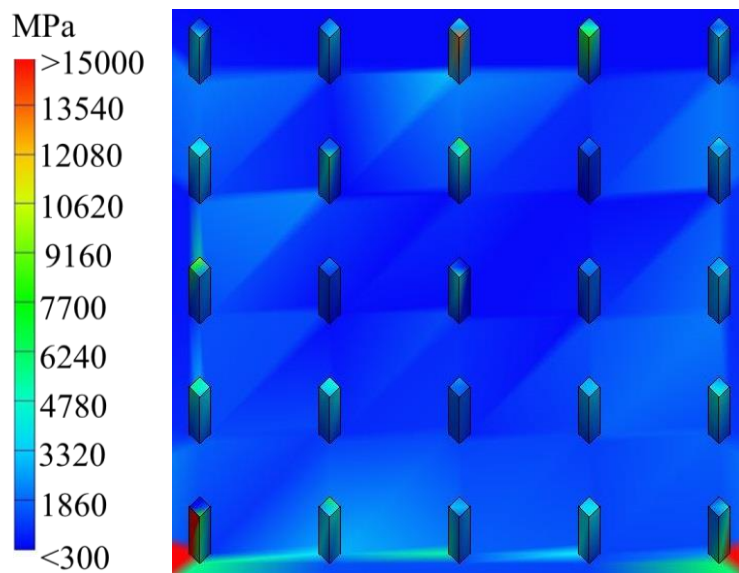


Figure 31: Shear stress for 1.2 mm microarray spacing with bottom gate

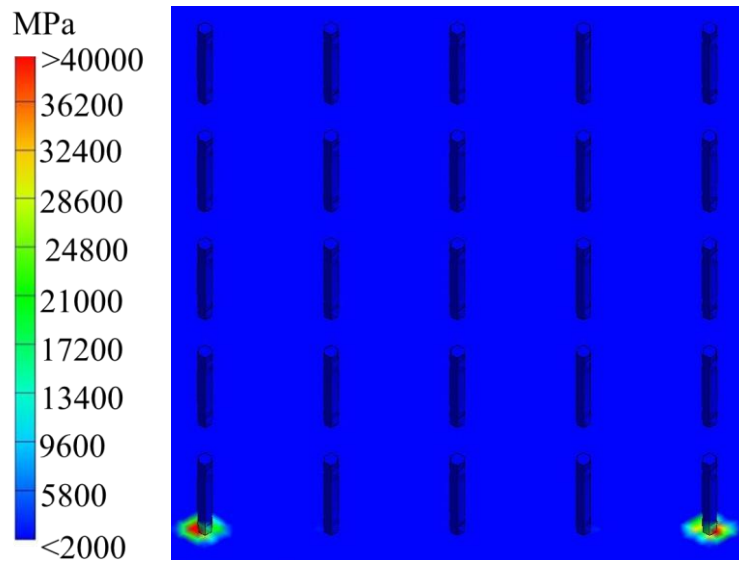


Figure 32: Shear stress for 1.7 mm microarray spacing with bottom gate

(D) Rheology of powder-polymer composite

PZT 52 vol. % WB50 rheology

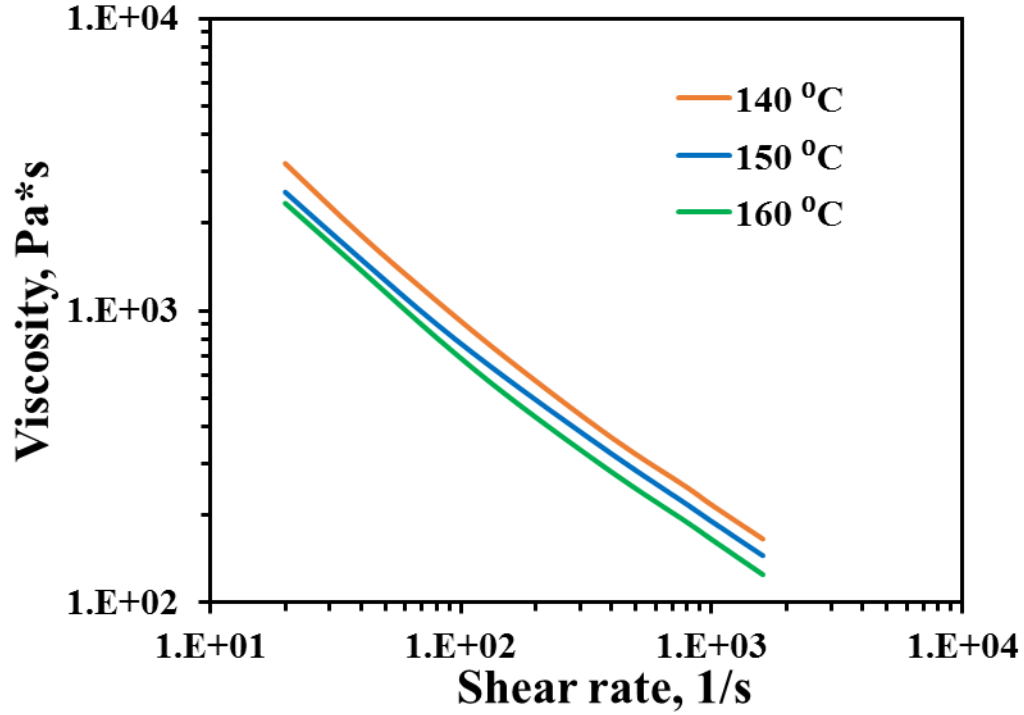


Figure 33: Measured viscosity of 52 vol. % PZT with WB50 multiccomponent binder

**Table 16:** Measured viscosity of 52 vol. % PZT with WB50 multiccomponent binder

140 °C		150 °C		160 °C	
Shear rate	Viscosity	Shear rate	Viscosity	Shear rate	Viscosity
s <sup>-1</sup>	Pa.s	s <sup>-1</sup>	Pa.s	s <sup>-1</sup>	Pa.s
20	3190.87	20	2543.93	20	2330.75
40	1814.43	40	1500.43	40	1375.73
80	1081.42	80	899.88	80	808.73
160	664.25	160	567.56	160	496.95
400	366.81	400	322.74	400	279.67
800	247.60	800	216.31	800	187.98
1000	215.91	1000	189.59	1000	164.44
1600	165.07	1600	144.82	1600	124.67

WB50 binder

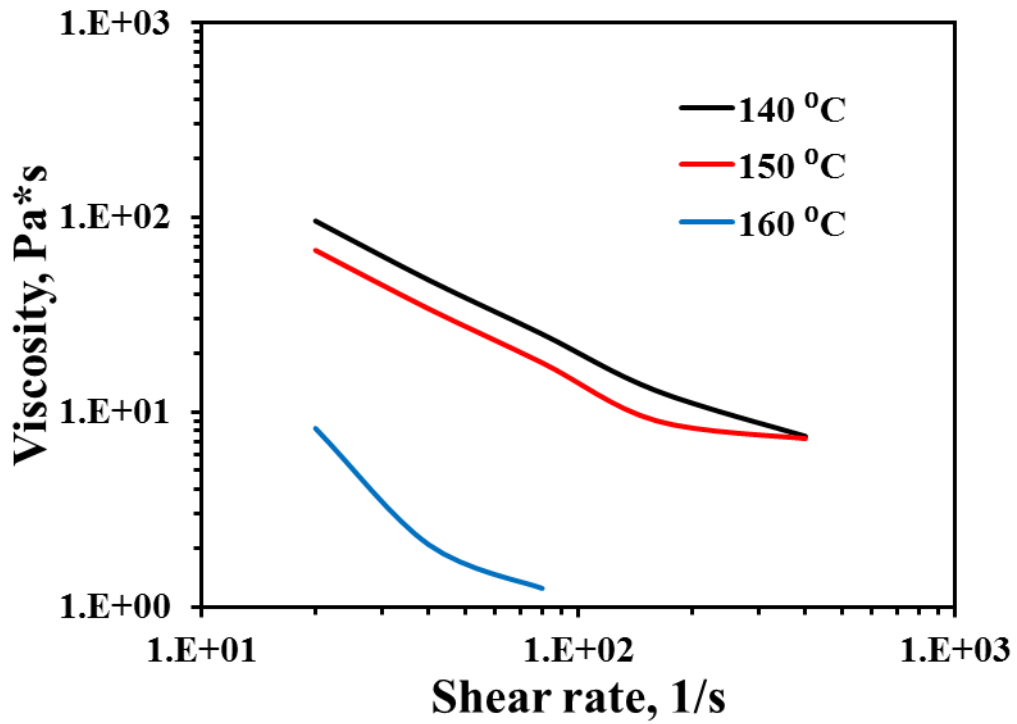


Figure 34: Measured viscosity of WB50 multicomponent binder

**Table 17: Measured viscosity of WB50 multicomponent binder**

140 °C		150 °C		160 °C	
Shear rate	Viscosity	Shear rate	Viscosity	Shear rate	Viscosity
s <sup>-1</sup>	Pa.s	s <sup>-1</sup>	Pa.s	s <sup>-1</sup>	Pa.s
<b>20</b>	95.73	20	67.67	20	8.24
<b>40</b>	47.57	40	33.85	40	2.08
<b>80</b>	25.12	80	17.89	80	1.24
<b>160</b>	12.90	160	9.04	160	-
<b>400</b>	7.51	400	7.30	400	-

## (E) LIST OF SYMBOLS

1.  $\Phi_p$  - volume fraction of powder
2.  $\Phi_b$  - volume fraction of binder
3.  $\Phi_c$  - volume fraction of composite
4.  $\rho_p$  - density of powder
5.  $\rho_b$  - density of binder
6.  $\rho_c$  - density of composite
7.  $v(T,p)$  - specific volume at a given temperature and pressure
8.  $v_0$  - specific volume at zero-gauge pressure,  $p$  - pressure,
9.  $C$  - constant, 0.0894
10.  $b_{1s}, b_{2s}, b_{3s}, b_{4s}, b_5, b_7, b_8, b_9$  - curve-fitted coefficients
11.  $b_{1m}, b_{2m}, b_{3m}, b_{4m}, b_5, b_6$  - curve-fitted coefficients
12.  $\eta_b$  - viscosity of binder
13.  $\Phi_p$  - volume fraction of powder
14.  $\Phi_{max}$  - maximum volume fraction
15.  $\gamma$  - shear rate
16.  $\tau^*$  - critical stress level at the transition to shear thinning
17.  $n$  - power law index in the high shear rate regime

18.  $T$  – temperature
19.  $T_t$  - volumetric transition temperature
20.  $T^*$ ,  $D_1$ ,  $A_1$  - curve-fitted coefficients
21.  $A_2$  - WLF constant, 51.6 K



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“Influence of feedstock property for estimates and measurements on powder injection molding of lead zirconate titanate”, *Powder Injection Moulding International*, vol 11 no. 4, pp 86-90